

MAJOR SITE PLAN MODIFICATION GRANDVIEW ROAD SUBDIVISION - PRIVATE WAY GRANDVIEW ROAD EXTENSION

PROJECT LOCATION: LOTS 2, 3, and 4 GRANDVIEW ROAD EXTENSION READING, MA 01867

SHEET INDEX

COVER SHEET EXISTING CONDITIONS (BY OTHERS) SV-1 PLAN OF LAND C-1 SITE AND TREE PRESERVATION PLAN C-2 C-3 EROSION AND SEDIMENT CONTROL PLAN GRADING AND DRAINAGE PLAN C-4 UTILITY AND ROADWAY PROFILE PLAN C-5 C-6 DETAILS SHEET 1

PROPERTY INFORMATION

DETAILS SHEET 2

RECORD OWNER LOTS 2, 3, & 4 GRANDVIEW, LLC GRANDVIEW ROAD EXTENSION 45 BEACON STREET READING, MA 01867 READING, MA 01867

COMBINED LOTS 2, 3, & 4 SINGLE FAMILY 15 (S-15) 45,132 S.F. (1.04 AC.±)

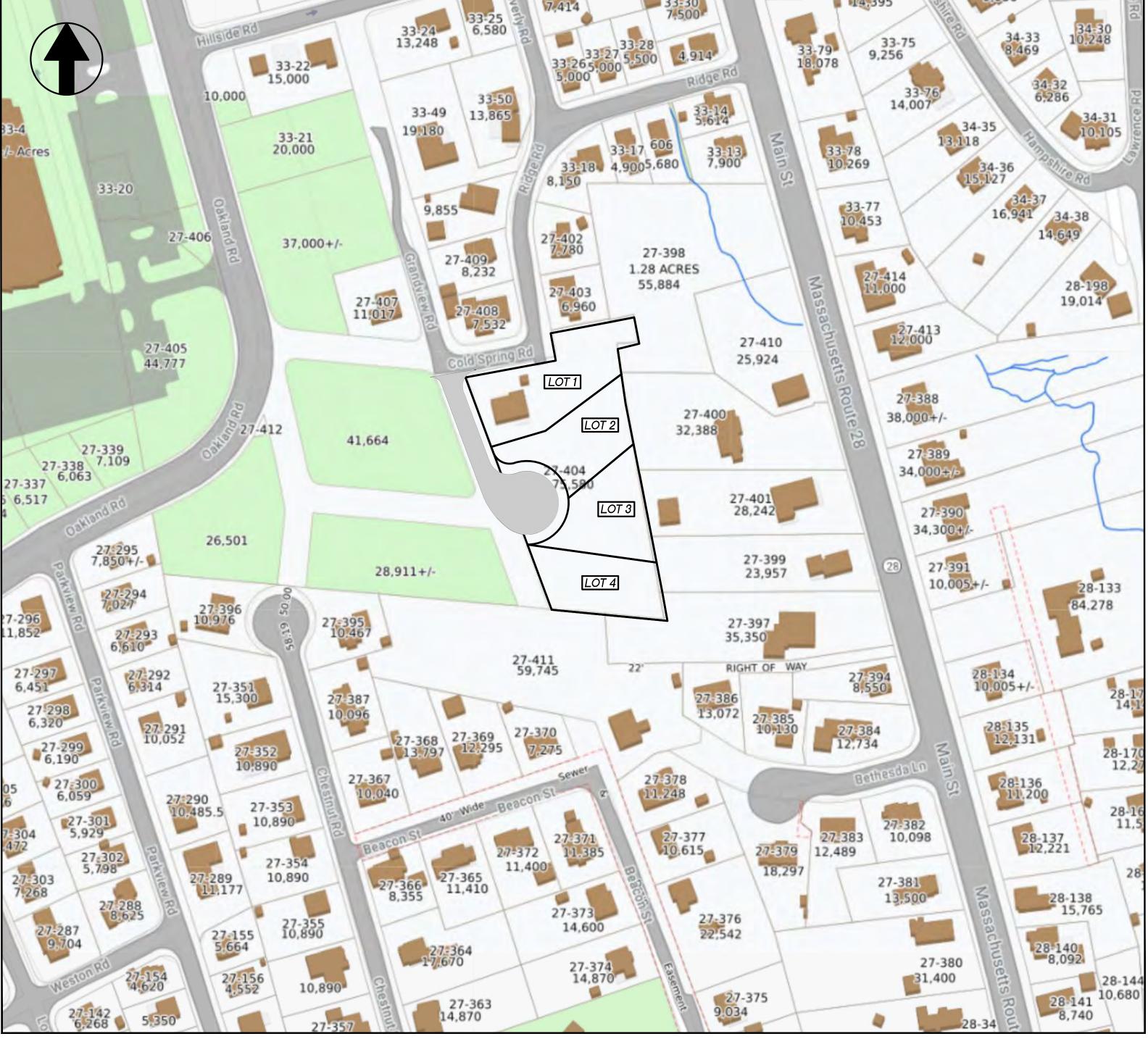
PARCEL ID
PART OF MAP 27, LOT 404

PLAN REFERENCES

- 1. BOUNDARY, TOPOGRAPHIC, AND PLANIMETRIC INFORMATION WAS OBTAINED FROM AN ON-THE-GROUND SURVEY PERFORMED AND COMPLETED BY PFS LAND SURVEYING, INC., DRAWING NUMBER SV-1, DATED 7/8/2020.
- 2. MIDDLESEX SOUTH REGISTRY OF DEEDS PLAN 754 OF YEAR 2022.

GENERAL NOTES

- 1. THE SUBDIVISION OF LAND FOR THIS PROJECT WAS APPROVED AND ENDORSED BY THE READING COMMUNITY PLANNING AND DEVELOPMENT COMMISSION (CPDC), AND THE SUBDIVISION WAS RECORDED WITH THE REGISTRY OF DEEDS ÀS PLAN 754 OF YEAR 2022.
- 2. THIS PLAN SET IS FOR THE APPROVAL OF A MAJOR SITE PLAN MODIFICATION. MODIFICATIONS INCLUDE REDESIGNING THE STORMWATER SYSTEM WITH ASSOCIATED SITE GRADING. EASEMENTS HAVE BEEN ADJUSTED AND THEREFORE WILL REQUIRE A NEW ENDORSED SET FOR RECORDING WITH THE REGISTRY.
- 3. TOPOGRAPHIC DATA IS ON THE NORTH AMERICAN VERTICAL DATUM OF 1988 (NAVD88).
- 4. UTILITY INFORMATION OBTAINED FROM THE REFERENCE SURVEY PLAN.
- 5. SOIL TESTS BY DEEP OBSERVATION HOLES WERE COMPLETED AND REPORTED BY ARMAND J. PORRAZZO (SE#1958) IN JULY 2020. SITE SOILS FROM THE NATURAL RESOURCES CONSERVATION SERVICE (NRCS) ONLINE WEB SOIL SURVEY DETERMINE THE SITE TO CONTAIN TWO (2) SOIL TYPES IDENTIFIED AS CANTON-CHARLTON-URBAN LAND COMPLEX WITH A HYDROLOGIC SOIL GROUP (HSG) "A" AND PAXTON FINE SANDY LOAM WITH A HSG "C".
- 6. THE SITE DOES NOT CONTAIN AREAS SUBJECT TO 1% ANNUAL CHANCE OF FLOODING AND IS IN ZONE "X" AS DETERMINED BY FEMA FLOOD INSURANCE RATE MAP (FIRM) 25017C0311E WITH AN EFFECTIVE DATE OF 6/4/2010.
- 7. THE SITE IS INLAND AND <u>NOT</u> LOCATED NEAR OR WITHIN THE FOLLOWING PROTECTED RESOURCE AREAS AS DETERMINED BY THE STATE OF MASSACHUSETTS ONLINE GIS MAPPING SYSTEM "OLIVER". - NATURAL HERITAGE OF ENDANGERED SPECIES
 - RIVERFRONT
 - CERTIFIED VERNAL POOLS
 - WELLHEAD PROTECTION ZONES
- 6. THE SITE DOES CONTAIN A SMALL PORTION OF BORDERING VEGETATED WETLANDS AND WERE DELINEATED BY LEC ENVIRONMENTAL CONSULTANTS, INC. IN JUNE 2020.



LOCUS MAP SCALE: 1" = 100'

PREPARED FOR: (APPLICANT) MICHAEL SALAMONE 45 BEACON STREET READING. MA 01867

PREPARED BY: **ENGINEERING** 28 HARBOR STREET, SUITE 204 DANVERS. MA 01923 (617) 877-3293

TOWN OF READING COMMUNITY PLANNING AND DEVELOPMENT COMMISSION DATE:

ABUTTER'S LIST (NOW OR FORMERLY)

27-367 27-368 27-369 27-370 27-371 27-372 27-377 27-378 27-378 27-386 27-385 27-386 27-387 27-397 27-397 27-398 27-397 27-398 27-399 27-400 27-401 27-402 27-403 27-404 27-405 27-407 27-408 27-409 27-410 27-411 33-13 33-14	14 BETHESDA 882 MAIN ST. 11 BETHESDA LN. 17 BETHESDA LN. 37 CHESTNUT RD. 884 MAIN ST. 43 CHESTNUT RD. 890 MAIN ST. MAIN ST. 896 MAIN ST. 908 MAIN ST. 900 MAIN ST. 26 RIDGE RD. 32 RIDGE RD. 4 COLDSPRING RD. OAKLAND RD. 23 GRANDVIEW RD. 31 RIDGE RD. 25 RIDGE RD. 912 MAIN ST. 45 BEACON ST. 930 MAIN ST. 934 MAIN ST.	TOWN OF READING READING MEMORIAL HIGH CUSOLITO ROBERT P JOANNE CUSOLITO CORAM GEOFFREY SUSAN G CORAM FONG ELAINE HATCH WILLIAM G SALAMONE ANGELO RICCI ANTHONY J JANET K GALLAGHER RICCI CROSBY JO ANN
27-409 27-410 27-411 33-13	25 RIDGE RD. 912 MAIN ST. 45 BEACON ST. 930 MAIN ST. 934 MAIN ST.	FONG ELAINE HATCH WILLIAM G SALAMONE ANGELO RICCI ANTHONY J JANET K GALLAGHER RICCI
33-16 33-17 33-18 33-19 33-23	8 RIDGE RD. 10 RIDGE RD. 14 RIDGE RD. OAKLAND RD. 23 RIDGE RD. 10 GRANDVIEW RD.	YAO RYAN S ALLEN KATHERINE D HEGARTY GERALD P ETAL TRS GERALD P HEGARTY REVOC TOWN OF READING SCHOOL DEPT. MESSINA—PEREZ KAREN E DRUID DAVID A PATRICIA E DRUID HILDRETH JOHN W JUDITH D HILDRETH

UTILITIES AND CONTACTS

CABLE

COMCAST CABLE CORPORATION 5 OMNI WAY CHELMSFORD, MA 01824 ATTN: TED QUINT 978-848-5163 ted_quint@comcast.com

NATIONAL GRID GAS 40 SYLVAN ROAD WALTHAM, MA 02451 ATTN: MELISSA OWENS 781-907-2845 melissa.owens@nationalgrid.com

WATER AND SEWER READING DPW 16 LOWELL ST. READING, MA 01867 781-942-9077

DEPARTMENT OF PUBLIC WORKS

READING MUNICIPAL LIGHT DEPARTMENT

READING DPW ENGINEERING DIVISION 16 LOWELL ST. READING, MA 01867 781-942-9082

385 MYLES STANDISH BLVD.

karen.m.mealey@verizon.com

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ATTN: PETER PRICE

781-942-6429

pprice@rmld.com

TELEPHONE

774-409-3160

VERIZON

CONSULTANTS

CIVIL ENGINEER

FODERA ENGINEERING 28 HARBOR ST., SUITE 204 DANVERS, MA 01923 ATTN: GIOVANNI FODERA, P.E. 617-877-3293 gfodera@foderaengineering.com

LAND SURVEYOR

PFS LAND SURVEYING, INC. 20 BALCH AVE. GROVELAND, MA 01834 ATTN: BRYAN PARMENTER, P.L.S. 508-446-0781 bryan@pfsland.com

DATE: MAY 10, 2024

REVISION BLOCK

REVISION SET	REVISION DATE	COMPLETED BY
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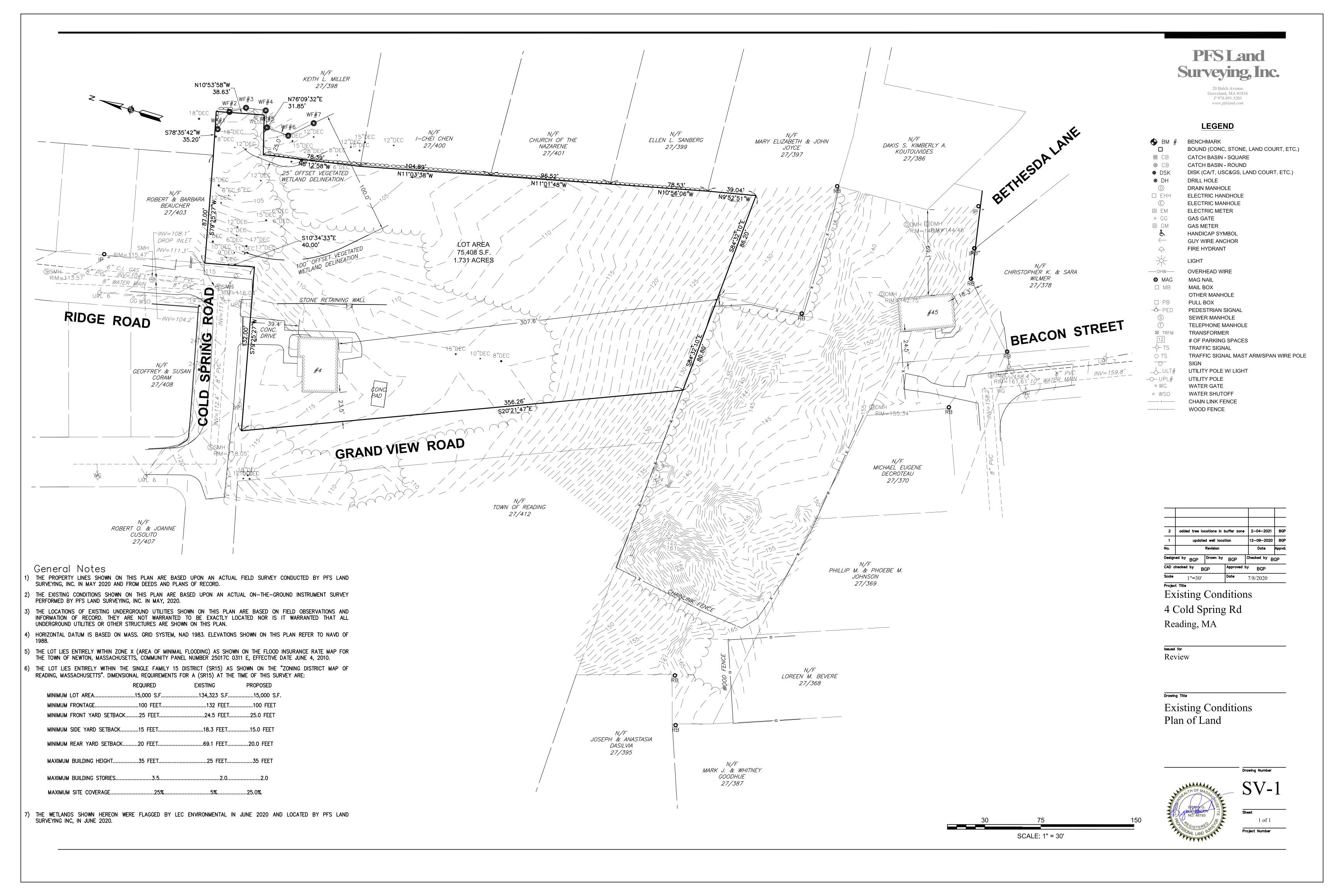


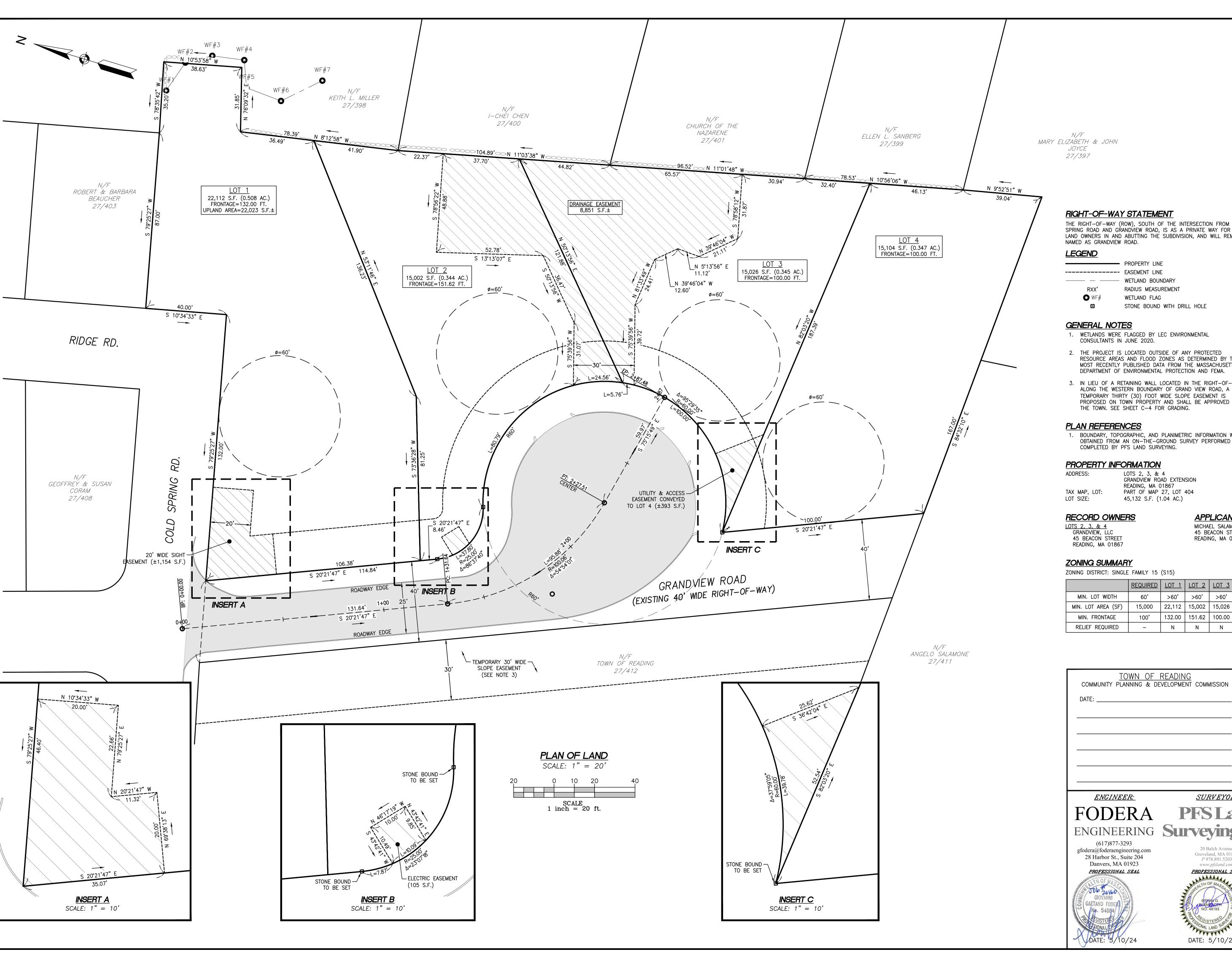
JOB NO.: 20160-14 SHEET TITLE: COVER SHEET

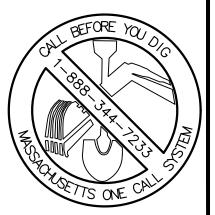
> SHEET NUMBER: C-0

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RIGHT-OF-WAY STATEMENT

THE RIGHT-OF-WAY (ROW), SOUTH OF THE INTERSECTION FROM COLD SPRING ROAD AND GRANDVIEW ROAD, IS AS A PRIVATE WAY FOR ALL LAND OWNERS IN AND ABUTTING THE SUBDIVISION, AND WILL REMAIN NAMED AS GRANDVIEW ROAD.

PROPERTY LINE ---- EASEMENT LINE WETLAND BOUNDARY RADIUS MEASUREMENT

WETLAND FLAG STONE BOUND WITH DRILL HOLE

GENERAL NOTES

1. WETLANDS WERE FLAGGED BY LEC ENVIRONMENTAL CONSULTANTS IN JUNE 2020.

- 2. THE PROJECT IS LOCATED OUTSIDE OF ANY PROTECTED RESOURCE AREAS AND FLOOD ZONES AS DETERMINED BY THE MOST RECENTLY PUBLISHED DATA FROM THE MASSACHUSETTS DEPARTMENT OF ENVIRONMENTAL PROTECTION AND FEMA.
- 3. IN LIEU OF A RETAINING WALL LOCATED IN THE RIGHT-OF-WAY ALONG THE WESTERN BOUNDARY OF GRAND VIEW ROAD, A TEMPORARY THIRTY (30) FOOT WIDE SLOPE EASEMENT IS PROPOSED ON TOWN PROPERTY AND SHALL BE APPROVED BY THE TOWN. SEE SHEET C-4 FOR GRADING.

PLAN REFERENCES

1. BOUNDARY, TOPOGRAPHIC, AND PLANIMETRIC INFORMATION WAS OBTAINED FROM AN ON-THE-GROUND SURVEY PERFORMED AND COMPLETED BY PFS LAND SURVEYING.

PROPERTY INFORMATION

LOTS 2, 3, & 4 GRANDVIEW ROAD EXTENSION READING, MA 01867 PART OF MAP 27, LOT 404 45,132 S.F. (1.04 AC.)

RECORD OWNERS

LOTS 2, 3, & 4 GRANDVIEW, LLC 45 BEACON STREET READING, MA 01867 APPLICANT
MICHAEL SALAMONE
45 BEACON ST.
READING, MA 01867

ZONING SUMMARY

ZONING DISTRICT: SINGLE FAMILY 15 (S15)

	REQUIRED	<u>LOT 1</u>	LOT 2	LOT 3	LOT 4
MIN. LOT WIDTH	60'	>60'	>60'	>60'	>60'
MIN. LOT AREA (SF)	15,000	22,112	15,002	15,026	15,104
MIN. FRONTAGE	100'	132.00	151.62	100.00	100.00
RELIEF REQUIRED	_	N	N	N	N

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MAJOR SITE PLAN
GRANDVIEW ROAD SUBDI

ENGINEER:

FODERA ENGINEERING Surveying, Inc.

(617)877-3293 gfodera@foderaengineering.com 28 Harbor St., Suite 204 Danvers, MA 01923



20 Balch Avenue Groveland, MA 01834 P 978.891.5203 www.pfsland.com PROFESSIONAL SEAL

DATE: 5/10/24

SURVEYOR:

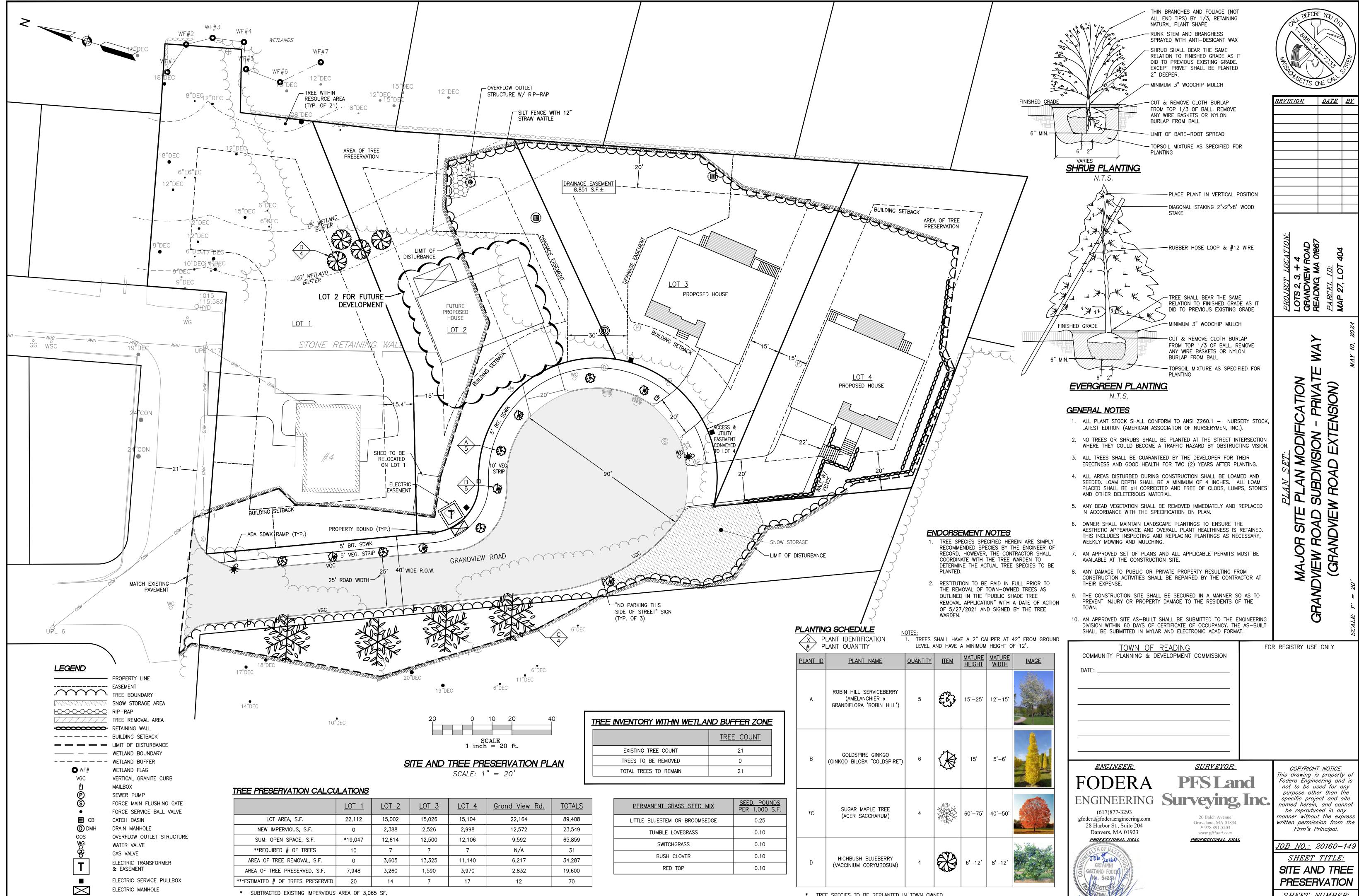
PFS Land

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> <u> JOB NO.:</u> 20160–148 SHEET TITLE: PLAN OF LAND

Firm's Principal.

SHEET NUMBER:



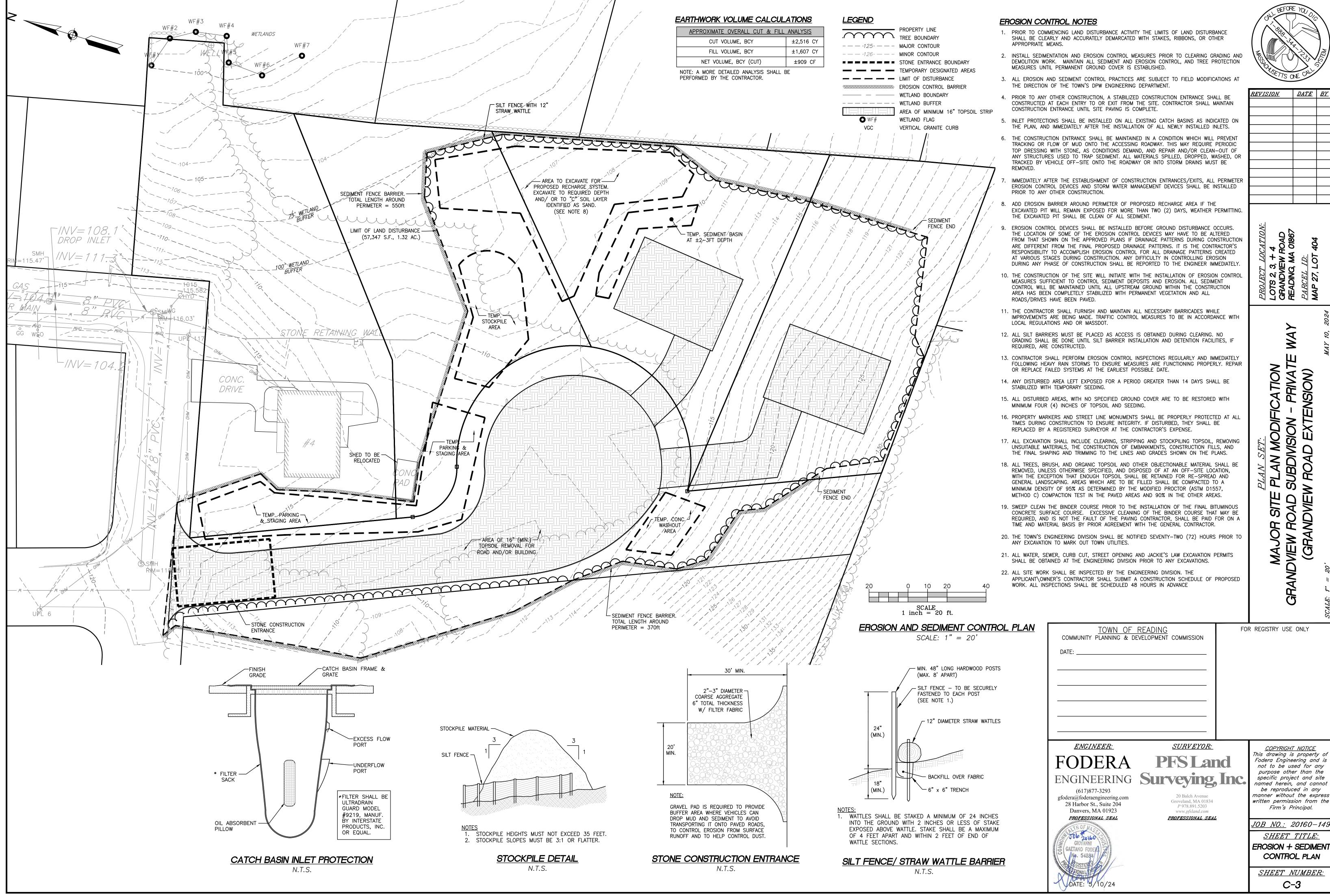
** BASED ON 1 TREE PER 2,000 S.F. OF OPEN SPACE PER SECTION 7.6.2.2 OF THE TOWN OF READING SUBDIVISION REGULATIONS.

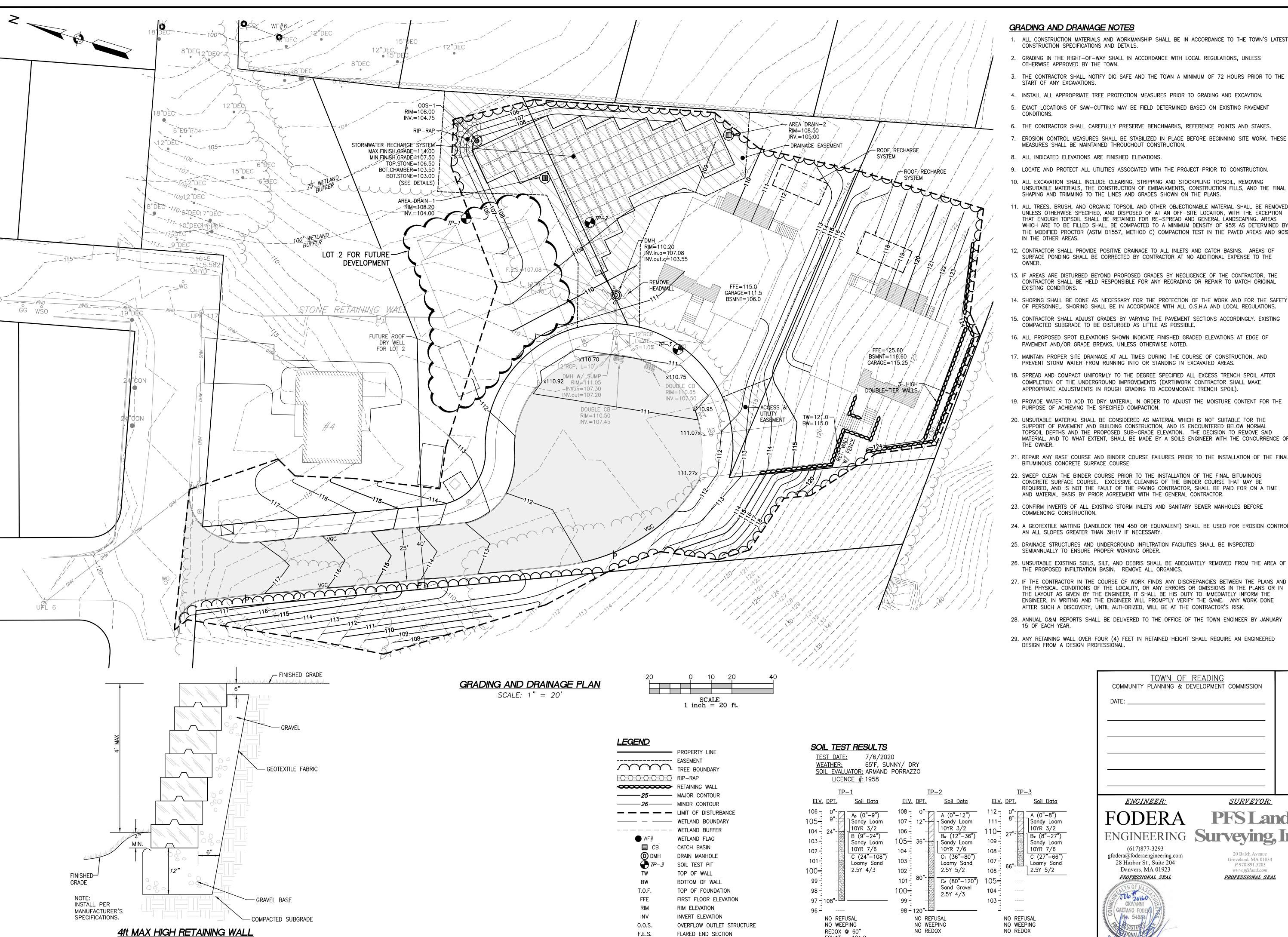
*** ESTIMATED BASED ON 1 TREE PER 225 S.F. (15'X15')

SHEET NUMBER:

C-2

* TREE SPECIES TO BE REPLANTED IN TOWN OWNED PROPERTY SHALL BE APPROVED BY THE TREE WARDEN.





N.T.S.

GRADING AND DRAINAGE NOTES

- 1. ALL CONSTRUCTION MATERIALS AND WORKMANSHIP SHALL BE IN ACCORDANCE TO THE TOWN'S LATEST CONSTRUCTION SPECIFICATIONS AND DETAILS.
- 2. GRADING IN THE RIGHT-OF-WAY SHALL IN ACCORDANCE WITH LOCAL REGULATIONS, UNLESS OTHERWISE APPROVED BY THE TOWN.
- 3. THE CONTRACTOR SHALL NOTIFY DIG SAFE AND THE TOWN A MINIMUM OF 72 HOURS PRIOR TO THE
- 4. INSTALL ALL APPROPRIATE TREE PROTECTION MEASURES PRIOR TO GRADING AND EXCAVTION.
- 5. EXACT LOCATIONS OF SAW-CUTTING MAY BE FIELD DETERMINED BASED ON EXISTING PAVEMENT
- CONDITIONS.
- EROSION CONTROL MEASURES SHALL BE STABILIZED IN PLACE BEFORE BEGINNING SITE WORK. THESE MEASURES SHALL BE MAINTAINED THROUGHOUT CONSTRUCTION.
- 8. ALL INDICATED ELEVATIONS ARE FINISHED ELEVATIONS.
- 9. LOCATE AND PROTECT ALL UTILITIES ASSOCIATED WITH THE PROJECT PRIOR TO CONSTRUCTION.
- 10. ALL EXCAVATION SHALL INCLUDE CLEARING, STRIPPING AND STOCKPILING TOPSOIL, REMOVING UNSUITABLE MATERIALS, THE CONSTRUCTION OF EMBANKMENTS, CONSTRUCTION FILLS, AND THE FINAL SHAPING AND TRIMMING TO THE LINES AND GRADES SHOWN ON THE PLANS.
- 11. ALL TREES, BRUSH, AND ORGANIC TOPSOIL AND OTHER OBJECTIONABLE MATERIAL SHALL BE REMOVED, UNLESS OTHERWISE SPECIFIED, AND DISPOSED OF AT AN OFF-SITE LOCATION, WITH THE EXCEPTION THAT ENOUGH TOPSOIL SHALL BE RETAINED FOR RE-SPREAD AND GENERAL LANDSCAPING. AREAS WHICH ARE TO BE FILLED SHALL BE COMPACTED TO A MINIMUM DENSITY OF 95% AS DETERMINED BY THE MODIFIED PROCTOR (ASTM D1557, METHOD C) COMPACTION TEST IN THE PAVED AREAS AND 90% IN THE OTHER AREAS.
- 12. CONTRACTOR SHALL PROVIDE POSITIVE DRAINAGE TO ALL INLETS AND CATCH BASINS. AREAS OF SURFACE PONDING SHALL BE CORRECTED BY CONTRACTOR AT NO ADDITIONAL EXPENSE TO THE
- 13. IF AREAS ARE DISTURBED BEYOND PROPOSED GRADES BY NEGLIGENCE OF THE CONTRACTOR, THE CONTRACTOR SHALL BE HELD RESPONSIBLE FOR ANY REGRADING OR REPAIR TO MATCH ORIGINAL EXISTING CONDITIONS.
- 14. SHORING SHALL BE DONE AS NECESSARY FOR THE PROTECTION OF THE WORK AND FOR THE SAFETY OF PERSONNEL. SHORING SHALL BE IN ACCORDANCE WITH ALL O.S.H.A AND LOCAL REGULATIONS.
- 15. CONTRACTOR SHALL ADJUST GRADES BY VARYING THE PAVEMENT SECTIONS ACCORDINGLY. EXISTING COMPACTED SUBGRADE TO BE DISTURBED AS LITTLE AS POSSIBLE.
- 16. ALL PROPOSED SPOT ELEVATIONS SHOWN INDICATE FINISHED GRADED ELEVATIONS AT EDGE OF PAVEMENT AND/OR GRADE BREAKS, UNLESS OTHERWISE NOTED.
- 17. MAINTAIN PROPER SITE DRAINAGE AT ALL TIMES DURING THE COURSE OF CONSTRUCTION, AND PREVENT STORM WATER FROM RUNNING INTO OR STANDING IN EXCAVATED AREAS.
- 18. SPREAD AND COMPACT UNIFORMLY TO THE DEGREE SPECIFIED ALL EXCESS TRENCH SPOIL AFTER COMPLETION OF THE UNDERGROUND IMPROVEMENTS (EARTHWORK CONTRACTOR SHALL MAKE
- 19. PROVIDE WATER TO ADD TO DRY MATERIAL IN ORDER TO ADJUST THE MOISTURE CONTENT FOR THE PURPOSE OF ACHIEVING THE SPECIFIED COMPACTION.
- 20. UNSUITABLE MATERIAL SHALL BE CONSIDERED AS MATERIAL WHICH IS NOT SUITABLE FOR THE SUPPORT OF PAVEMENT AND BUILDING CONSTRUCTION, AND IS ENCOUNTERED BELOW NORMAL TOPSOIL DEPTHS AND THE PROPOSED SUB-GRADE ELEVATION. THE DECISION TO REMOVE SAID MATERIAL, AND TO WHAT EXTENT, SHALL BE MADE BY A SOILS ENGINEER WITH THE CONCURRENCE OF THE OWNER.
- 21. REPAIR ANY BASE COURSE AND BINDER COURSE FAILURES PRIOR TO THE INSTALLATION OF THE FINAL BITUMINOUS CONCRETE SURFACE COURSE.
- 22. SWEEP CLEAN THE BINDER COURSE PRIOR TO THE INSTALLATION OF THE FINAL BITUMINOUS CONCRETE SURFACE COURSE. EXCESSIVE CLEANING OF THE BINDER COURSE THAT MAY BE REQUIRED, AND IS NOT THE FAULT OF THE PAVING CONTRACTOR, SHALL BE PAID FOR ON A TIME AND MATERIAL BASIS BY PRIOR AGREEMENT WITH THE GENERAL CONTRACTOR.
- 23. CONFIRM INVERTS OF ALL EXISTING STORM INLETS AND SANITARY SEWER MANHOLES BEFORE COMMENCING CONSTRUCTION.
- 24. A GEOTEXTILE MATTING (LANDLOCK TRM 450 OR EQUIVALENT) SHALL BE USED FOR EROSION CONTROL AN ALL SLOPES GREATER THAN 3H:1V IF NECESSARY.
- 25. DRAINAGE STRUCTURES AND UNDERGROUND INFILTRATION FACILITIES SHALL BE INSPECTED
- SEMIANNUALLY TO ENSURE PROPER WORKING ORDER.
- 26. UNSUITABLE EXISTING SOILS, SILT, AND DEBRIS SHALL BE ADEQUATELY REMOVED FROM THE AREA OF THE PROPOSED INFILTRATION BASIN. REMOVE ALL ORGANICS.
- THE PHYSICAL CONDITIONS OF THE LOCALITY, OR ANY ERRORS OR OMISSIONS IN THE PLANS OR IN THE LAYOUT AS GIVEN BY THE ENGINEER, IT SHALL BE HIS DUTY TO IMMEDIATELY INFORM THE ENGINEER, IN WRITING AND THE ENGINEER WILL PROMPTLY VERIFY THE SAME. ANY WORK DONE AFTER SUCH A DISCOVERY, UNTIL AUTHORIZED, WILL BE AT THE CONTRACTOR'S RISK.
- 28. ANNUAL O&M REPORTS SHALL BE DELIVERED TO THE OFFICE OF THE TOWN ENGINEER BY JANUARY 15 OF EACH YEAR.
- 29. ANY RETAINING WALL OVER FOUR (4) FEET IN RETAINED HEIGHT SHALL REQUIRE AN ENGINEERED

<u>REVISION</u>	<u>DATE</u>	<u>BY</u>

PLAI SUBE V RO

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COMMUNITY PLANNING & DEVELOPMENT COMMISSION

TOWN OF READING

ENGINEER:

SURVEYOR:

FODERA ENGINEERING Surveying, Inc.

GAETANO FODER

ESHWT = 101.0

gfodera@foderaengineering.com 28 Harbor St., Suite 204 Danvers, MA 01923 PROFESSIONAL SEAL

20 Balch Avenue

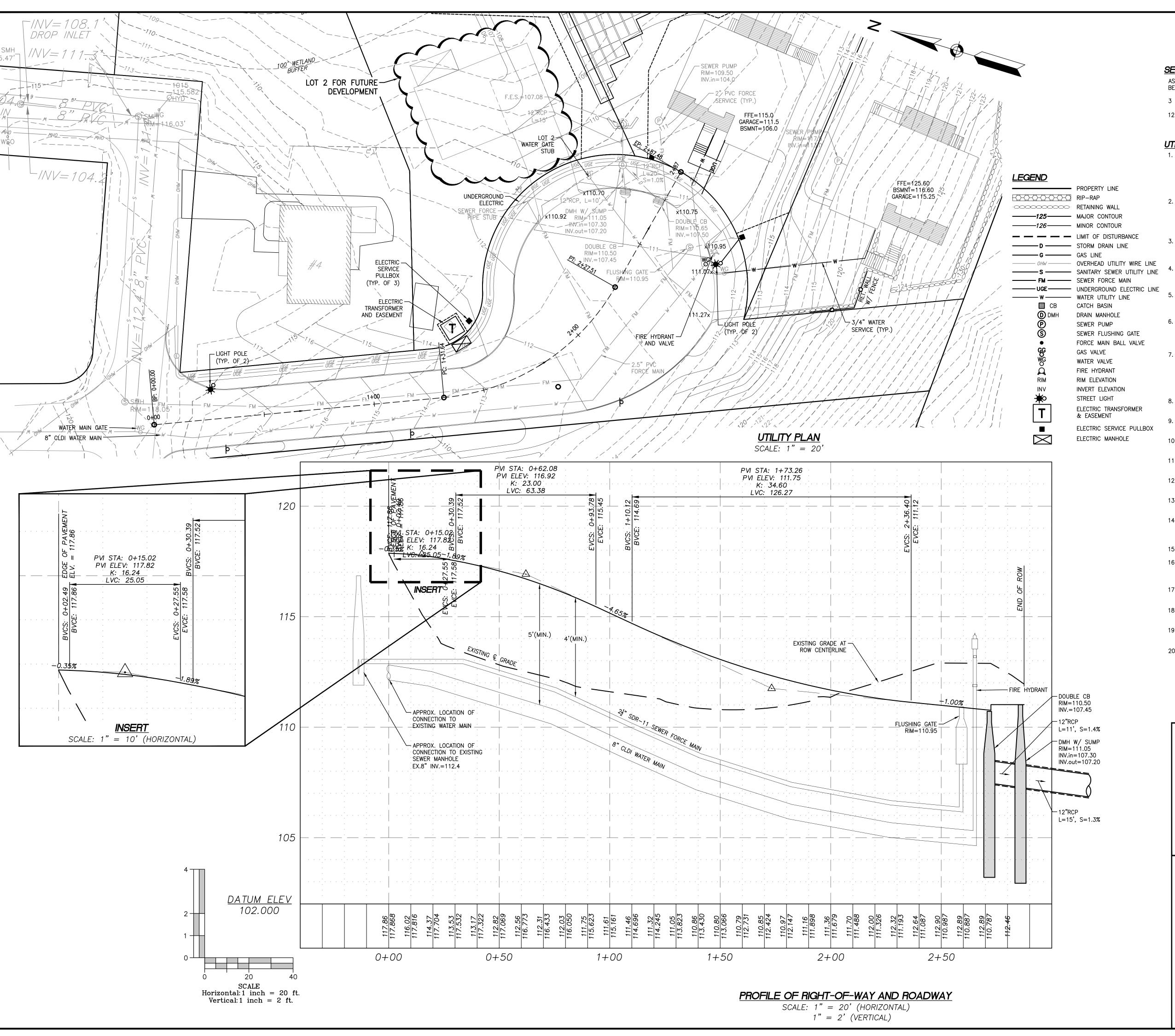
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> JOB NO.: 20160-14 SHEET TITLE:

GRADING AND

DRAINAGE PLAN SHEET NUMBER:



SEWAGE CALCULATIONS

ASSUMPTIONS MADE FOR EACH PROPOSED HOUSE TO CONTAIN FOUR (4) BEDROOMS. CALCULATIONS BELOW ARE IN ACCORDANCE TO 310 CMR 15.00.

3 NEW HOUSES * 4 BEDROOMS PER HOUSE = 12 BEDROOMS ADDED

12 BEDROOMS * 110 GAL/DAY = 1,320 GAL/DAY OF ADDED SEWAGE

UTILITY NOTES

- 1. CONTRACTOR IS TO VERIFY THE LOCATION OF ALL EXISTING UTILITIES PRIOR TO CONSTRUCTION AND ENSURE NO CONFLICTS EXIST WITH PROPOSED IMPROVEMENTS. NOTIFY ENGINEER IMMEDIATELY IF UTILITIES ARE LOCATED DIFFERENTLY THAN SHOWN. THE CONTRACTOR SHALL COORDINATE WITH EACH RESPECTIVE UTILITY COMPANY IN ORDER TO RELOCATE IF NEEDED IN CONFORMANCE WITH THEIR GUIDELINES.
- 2. CONTRACTOR SHALL NOTIFY AND COORDINATE WITH THE APPROPRIATE UTILITY COMPANY PRIOR TO THE REMOVAL OF INDICATED UTILITIES ON SITE. CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ANY PERMITS REQUIRED FOR DEMOLITION AND HAUL OFF FROM THE APPROPRIATE AUTHORITIES.
- 3. THE DEPARTMENT OF PUBLIC WORKS OR APPLICABLE GOVERNING DEPARTMENT MUST AUTHORIZE AND PERMIT TO CONSTRUCT, ALTER OR MODIFY A WATER OR SEWER LINE.
- AT THE COMPLETION OF THE WATER AND/OR SEWER CONSTRUCTION AND PRIOR TO RECORDING THE FINAL PLAT, THE CONTRACTOR WILL FURNISH THE WATER SYSTEM INSPECTOR RECORD DRAWINGS OF THE PROJECT.
- 5. BUILDING CONTRACTOR SHALL BE RESPONSIBLE FOR COORDINATION WITH THE GAS COMPANY FOR THE CONSTRUCTION OF THE GAS LINE BETWEEN METER AND MAIN.
- 6. BUILDING CONTRACTOR SHALL BE RESPONSIBLE FOR COORDINATION WITH THE POWER COMPANY FOR THE CONSTRUCTION OF ELECTRICAL CONDUIT TO PROVIDE SERVICE AND IF A TRANSFORMER IS REQUIRED TO BE INSTALLED.
- 7. THE CONTRACTOR SHALL BE RESPONSIBLE FOR VERIFYING, PRIOR TO CONSTRUCTION, ALL EXISTING LOCATIONS AND INVERT ELEVATIONS OF SANITARY SEWERS, STORM DRAINAGE, AND WATER MAINS. IF ANY INVERT ELEVATION VARIES MORE THAN 0.1 FT. FROM RECORD ELEVATIONS, THE CONTRACTOR SHALL NOTIFY THE ENGINEER IMMEDIATELY. WORK SHALL NOT PROCEED UNTIL THE CONTRACTOR IS NOTIFIED BY THE ENGINEER.
- 8. CONNECT TO EXISTING UTILITIES AND INSTALL UTILITIES IN COMPLIANCE WITH REQUIREMENTS OF APPROPRIATE JURISDICTIONAL AGENCIES.
- COORDINATE WITH BUILDING PLANS TO ASSURE ACCURACY OF UTILITY CONNECTIONS AND COMPLIANCE WITH LOCAL CODES.
- 10. ALL SEWERS TO BE MAINTAINED THROUGHOUT CONSTRUCTION, INCLUDING CLEANING OF ANY SILT OR DEBRIS ACCUMULATED IN STRUCTURES.
- 11. ALL SURPLUS EXCAVATED MATERIAL FROM THE TRENCH SHALL BE DISPOSED OFF THE SITE BY CONTRACTOR.
- 12. TRENCHING SHOULD BE CONDUCTED IN ACCORDANCE WITH ALL OSHA REGULATIONS.
- 13. COORDINATE EXACT TRENCHING, ROUTING, AND POINT OF TERMINATION WITH ALL UTILITY COMPANIES.
- 14. BACKFILL MATERIAL SHALL BE SUITABLE MATERIAL IN COMPLIANCE WITH THE TOWN OF DANVERS AND/OR THE MASSACHUSETTS DEPARTMENT OF TRANSPORTATION (MASSDOT).
- 15. WATER MAIN SHALL HAVE A MINIMUM COVER OF FIVE (5) FEET.
- 16. THE SANITARY SEWER AND POTABLE WATER LINES ARE TO BE SEPARATED BY AT LEAST 10 FEET HORIZONTALLY, OR THE POTABLE WATER LINE SHALL BE AT LEAST 18 INCHES VERTICALLY ABOVE THE SANITARY SEWER.
- 17. CONTRACTOR TO RECONFIGURE PROPOSED ELECTRIC/TELEPHONE/CABLE CONDUITS AS NECESSARY TO AVOID CONFLICT WITH TREES/LANDSCAPING.
- 18. THRUST BLOCKS TO BE PLACED AT ALL BEND LOCATIONS WITHIN THE POTABLE WATER LINES. SEE DETAIL SHEETS.
- 19. ALL UTILITIES SHALL BE APPROVED MATERIALS AND INSTALLED IN ACCORDANCE WITH THE DEPARTMENT OF PUBLIC WORKS STANDARDS.
- 20. THE TOWN'S ENGINEERING DIVISION SHALL BE NOTIFIED SEVENTY-TWO (72) HOURS PRIOR TO ANY EXCAVATION TO MARK OUT TOWN UTILITIES.

UTILITY AND ROADWAY PROFILE PLAN

SCALE: 1" = 20' (HORIZONTAL)

TOWN OF READING COMMUNITY PLANNING & DEVELOPMENT COMMISSION	FOR REGISTRY USE ONLY
DATE:	

ENGINEER:

FODERA PFSLand

ENGINEERING Surveying, Inc (617)877-3293

(617)877-3293 gfodera@foderaengineering.com 28 Harbor St., Suite 204 Danvers, MA 01923 PROFESSIONAL SEAL

> JOB ZOLGO GIOVANNI

GAETANO FODER

Groveland, MA 01834 P 978.891.5203 www.pfsland.com PROFESSIONAL SEAL

20 Balch Avenue

SURVEYOR:

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MAJOR SITE PL GRANDVIEW ROAD SU (GRANDVIEW F

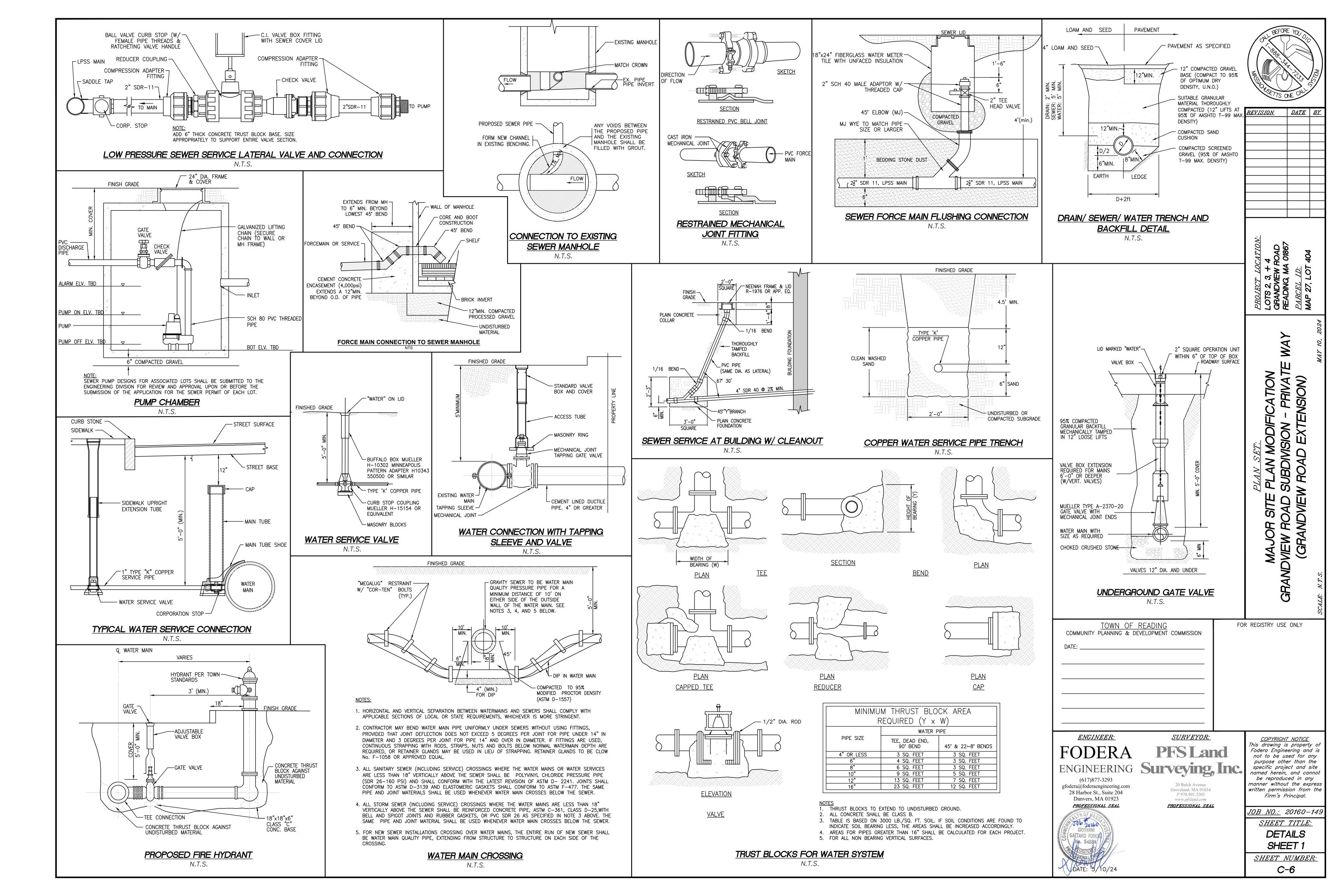
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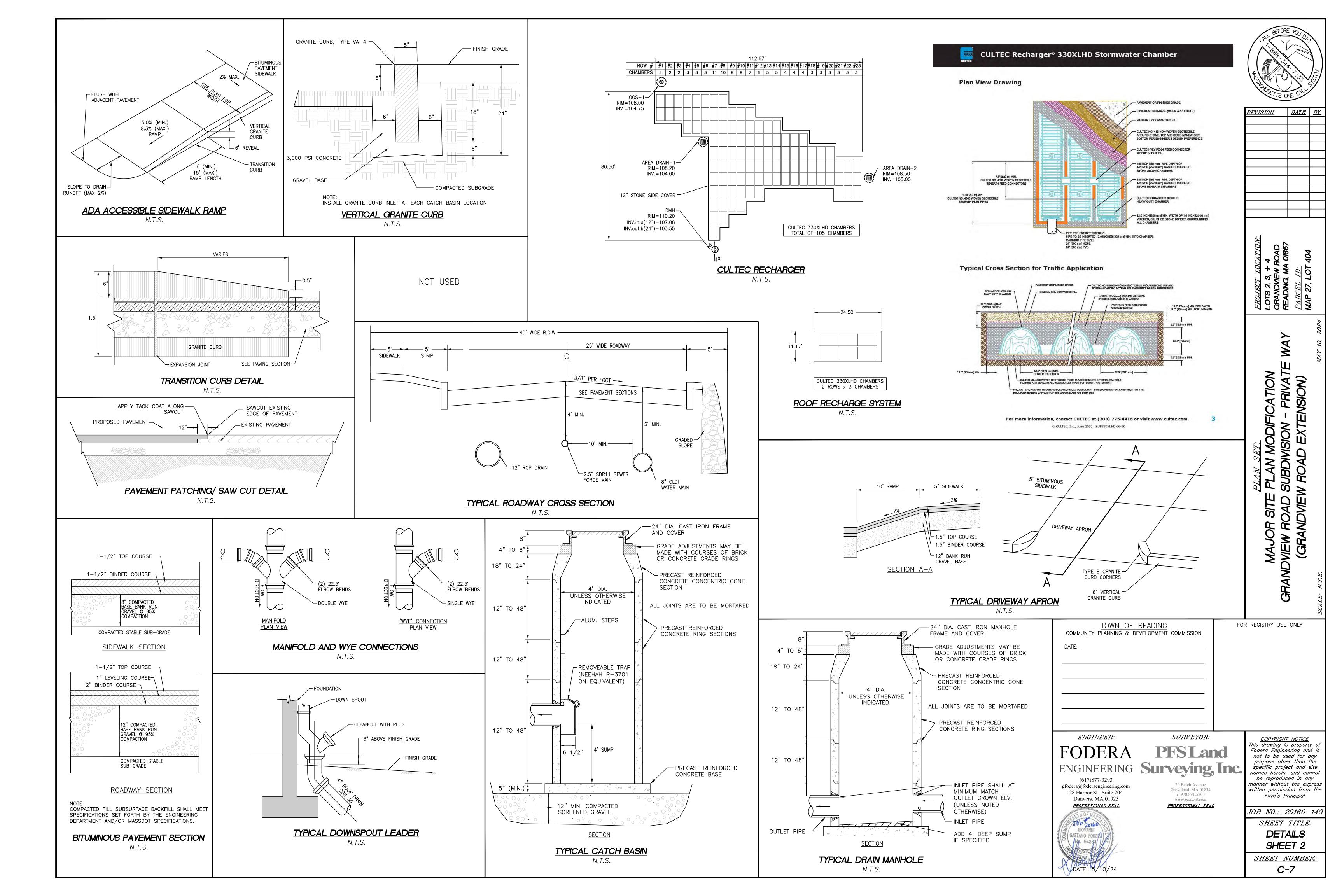
JOB NO.: 20160-149

SHEET TITLE:
UTILITY + ROADWAY

SHEET NUMBER:
C-5

PROFILE PLAN





FODERA ENGINEERING

28 Harbor Street, Suite 204 Danvers, MA 01923 Tel: (617) 992-8492

contact@foderaengineering.com

May 13, 2024

To: Andrew MacNichol, Community Development Director
 Town of Reading
 Community Planning and Development Commission
 16 Lowell Street
 Reading, MA 01867

RE: GRANDVIEW ROAD SUBDIVISION SITE PLAN MODIFICATIONS 4 COLD SPRING ROAD READING, MA 01867

To Mr. MacNichol.

The project at 4 Cold Spring Road known as Grandview Road Subdivision was originally approved by the Community Planning and Development Commission (CPDC) in 2021. A few years later, the project underwent a design modification to the stormwater system and roadway grading and was re-approved by the CPDC in 2023 as a Major Modification. The project commenced construction and the roadway with associated utilities were constructed along with the infiltration pond. However, the project has come to a halt and the plans have been modified so that the infiltration system matches the design from the 2021 original approved plans. Summaries of plan designs below:

2021 Approved Plans

- 4-Lot subdivision including the existing dwelling at 4 Cold Spring Road. Proposed to construct three (3) new houses along the approved roadway.
- Roadway cul-de-sac was designed at an approximate elevation of 113.
- Stormwater system consisted of multiple catch basins in the cul-de-sac and directed to an underground infiltration system within Lots 2 and 3.

2023 Approved Plans

- Property lines for the 4-lot subdivision remained unchanged. New proposal to keep Lot 2
 undeveloped with potential for future development. Lots 3 and 4 will be developed as new singlefamily dwellings.
- Roadway cul-de-sac was regraded and lowered by two (2) feet to an approximate elevation of
- Stormwater system was redesigned to collect runoff at the end of the cul-de-sac and empty out into an infiltration pond.

2024 Modified Plans

- Property lines remain unchanged, and Lot 2 will remain undeveloped with the potential for future development.
- Grading of roadway and cul-de-sac will remain unchanged and has been constructed according to the plans from 2023.
- Stormwater system will remain with catch basins at the end of the cul-de-sac but the infiltration pond will be modified to an underground infiltration system, similar to the approved plans in 2021.

Additional modifications between 2021 and 2024 plans

- Increased building footprints.
 - o Lot 3 will remain to have a separate roof runoff recharge system.
 - Lot 4 roof runoff previously was intended to be directed to the overall infiltration system.
 This has been modified to have a separate roof runoff recharge system on-site.
- Tree lines for Lots 3 & 4 were shifted back to create more lawn and less wooded surface.
- Although larger building footprints are implemented and the tree line creates more lawn and less
 wooded surface, there is no substantial change in runoff calculations. This is due to Lot 4 being
 modified to having its own roof runoff recharge system.
- The as-built roadway and drainage infrastructure are easily incorporated into the new drainage system with the associated elevations making a feasible design.

There are no new design waivers being requested for the modification.

Please accept this submittal as formal request for review. Please do not hesitate to call or email me shall you have any questions, comments, or concerns.

Sincerely yours,

Giovanni Fodera, PE, LSIT

President | Principal Engineer

FODERA Engineering

Attachments:

- Major Site Plan Modification Grandview Road Subdivision, dated May 10, 2024.
- Post-Development Runoff Summary & Calculations, dated May 10, 2024.

Cc: Michael Salamone

Frank Lanzillo

FODERA ENGINEERING

28 Harbor Street, Suite 204 Danvers, MA 01923

Tel: (617) 992-8492 contact@foderaengineering.com

May 13, 2024

Peak Rate of Discharge Summary

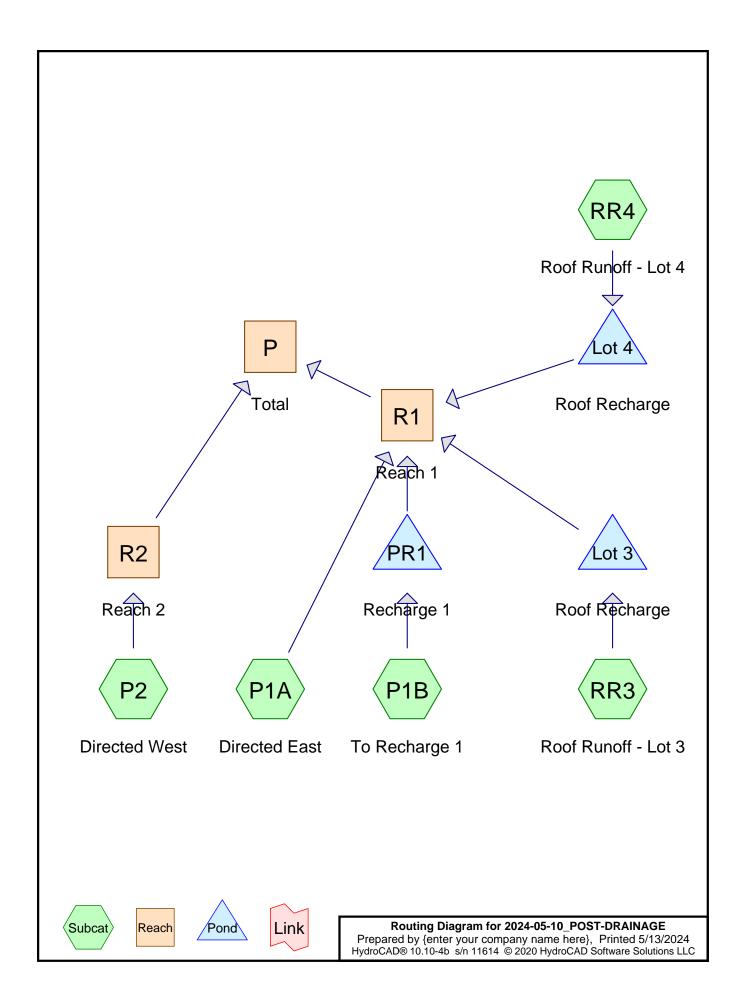
PEAK RATE OF DISCHARGE, cubic-feet per second								
	Rea	ch R1	Reac	h R2	Σ Reach R1 & R2			
Storm	Pre-	Post-	Pre-	Post-	Pre-	Post-		
Intensity	Conditions	Conditions	Conditions	Conditions	Conditions	Conditions		
2-year Storm 3.31"	0.24	0.01	0.52	0.03	0.65	0.03		
10-year Storm 5.22"	1.40	0.31	1.29	0.07	2.57	0.34		
25-year Storm 6.41"	2.38	0.73	1.81	0.09	4.05	0.78		
100-year Storm 8.24"	4.12	*4.64	2.65	0.13	6.57	4.68		

^{*} Increase at R1 but sum of the overall site (same watershed area) is less in the post-conditions.

Sincerely yours,

Giovanni Fodera, PE, LSIT President | Principal Engineer

FODERA Engineering



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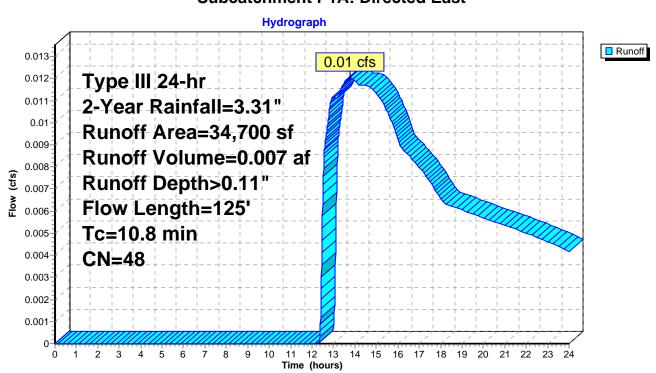
Summary for Subcatchment P1A: Directed East

Runoff = 0.01 cfs @ 13.79 hrs, Volume= 0.007 af, Depth> 0.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.31"

_	Α	rea (sf)	CN I	Description						
*		2,854	98	Impervious						
		14,380	39	>75% Grass cover, Good, HSG A						
		11,288	30	Woods, Good, HSG A						
		3,734	74	>75% Gras	s cover, Go	ood, HSG C				
		111	70	Woods, Good, HSG C						
_		2,333	80 :	>75% Gras	s cover, Go	ood, HSG D				
		34,700	48 \	Neighted A	verage					
		31,846	9	91.78% Pei	rvious Area					
		2,854		3.22% Impe	ervious Area	a				
	Tc	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	10.0	50	0.1400	0.08		Sheet Flow, Sheet Flow Woods				
						Woods: Dense underbrush n= 0.800 P2= 3.10"				
	8.0	75	0.1067	1.63		Shallow Concentrated Flow, Concentrated Woods				
_						Woodland Kv= 5.0 fps				
	10.8	125	Total							

Subcatchment P1A: Directed East



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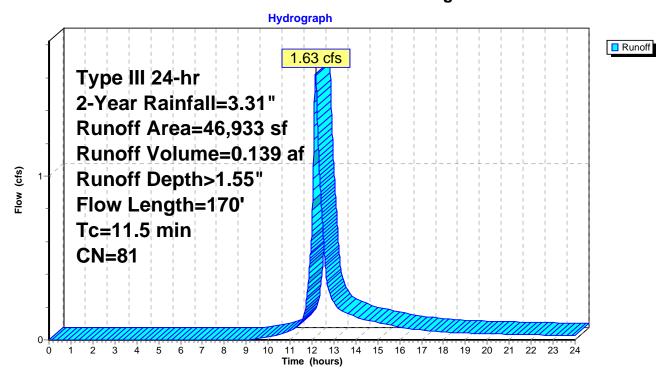
Summary for Subcatchment P1B: To Recharge 1

Runoff = 1.63 cfs @ 12.16 hrs, Volume= 0.139 af, Depth> 1.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.31"

	Δ	rea (sf)	CN	Description						
*		16,120	98	Impervious						
		989	39	>75% Gras	s cover, Go	ood, HSG A				
		21,312	74	>75% Gras	s cover, Go	ood, HSG C				
		8,215	70	Woods, Go	od, HSG C					
		297	80	>75% Gras	s cover, Go	ood, HSG D				
46,933 81 Weighted Average										
		30,813		65.65% Pe	rvious Area					
		16,120		34.35% lm _l	pervious Ar	ea				
	_									
	Tc	Length	Slope		Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	10.0	50	0.1400	0.08		Sheet Flow, Wood Sheet Flow				
						Woods: Dense underbrush n= 0.800 P2= 3.10"				
	1.5	120	0.0750	1.37		Shallow Concentrated Flow, Woods Concentrated Flow				
_						Woodland Kv= 5.0 fps				
	11.5	170	Total							

Subcatchment P1B: To Recharge 1



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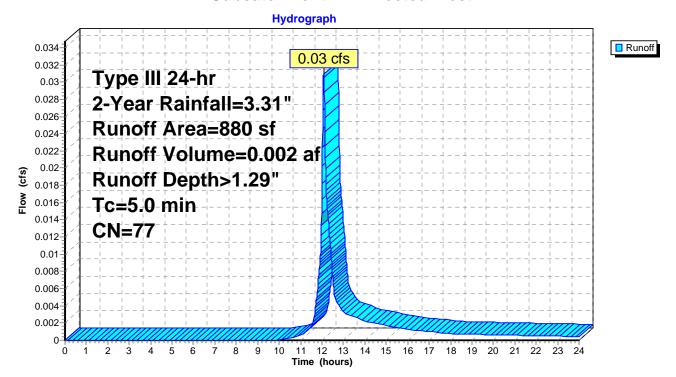
Summary for Subcatchment P2: Directed West

Runoff = 0.03 cfs @ 12.08 hrs, Volume= 0.002 af, Depth> 1.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.31"

_	Α	rea (sf)	CN	Description						
Ī		473	74	>75% Grass cover, Good, HSG C						
_		407	80	>75% Gras	s cover, Go	od, HSG D				
		880	77	Weighted A	verage					
		880		100.00% Pervious Area						
	Tc	Length	Slope	,	Capacity	Description				
_	(min)	(feet)	(ft/ft	(ft/sec)	(cfs)					
	5.0					Direct Entry				

Subcatchment P2: Directed West



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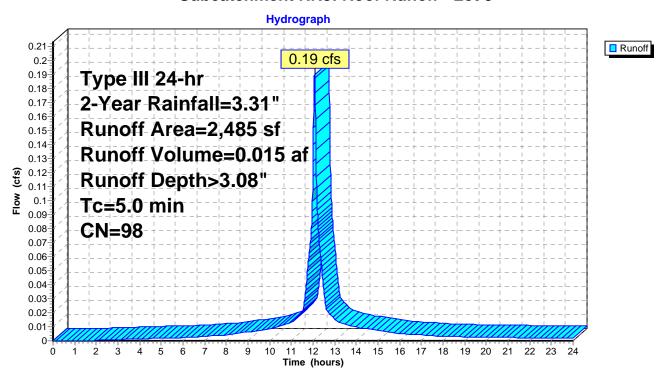
Summary for Subcatchment RR3: Roof Runoff - Lot 3

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.015 af, Depth> 3.08"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.31"

	Α	rea (sf)	CN	Description			
*		2,485	98	Roof			
		2,485		100.00% Impervious Area			
	Tc	Length	Slope	Velocity	Capacity	Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·	
	5.0					Direct Entry,	

Subcatchment RR3: Roof Runoff - Lot 3



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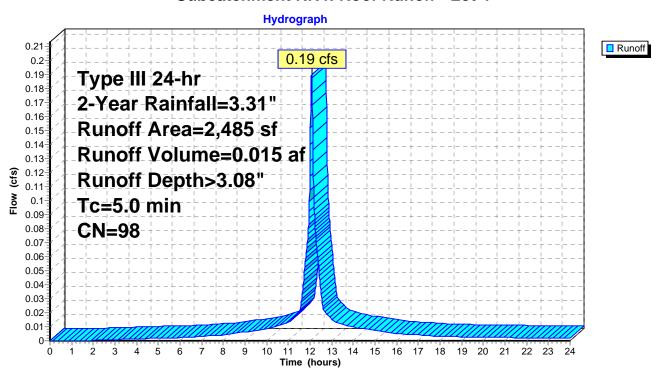
Summary for Subcatchment RR4: Roof Runoff - Lot 4

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.015 af, Depth> 3.08"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.31"

	Α	rea (sf)	CN	Description			
*		2,485	98	Roof			
		2,485		100.00% Impervious Area			
	Tc	Length	Slope	Velocity	Capacity	Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·	
	5.0					Direct Entry,	

Subcatchment RR4: Roof Runoff - Lot 4



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Summary for Reach P: Total

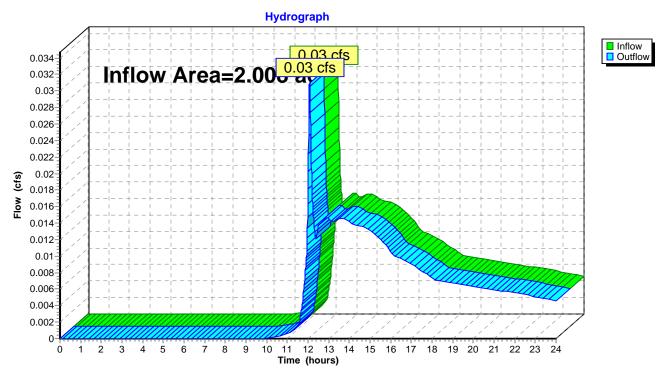
Inflow Area = 2.008 ac, 27.37% Impervious, Inflow Depth > 0.06" for 2-Year event

0.03 cfs @ 12.08 hrs, Volume= Inflow 0.009 af

0.03 cfs @ 12.08 hrs, Volume= Outflow 0.009 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Reach P: Total



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Summary for Reach R1: Reach 1

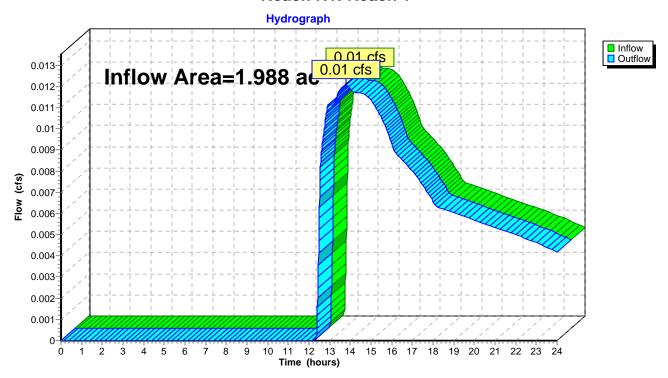
1.988 ac, 27.65% Impervious, Inflow Depth > 0.04" for 2-Year event Inflow Area =

0.01 cfs @ 13.79 hrs, Volume= Inflow 0.007 af

0.01 cfs @ 13.79 hrs, Volume= Outflow 0.007 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Reach R1: Reach 1



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Summary for Reach R2: Reach 2

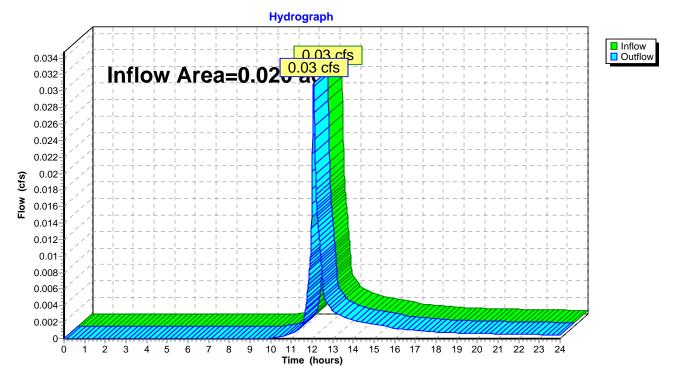
0.00% Impervious, Inflow Depth > 1.29" for 2-Year event Inflow Area = 0.020 ac,

0.03 cfs @ 12.08 hrs, Volume= Inflow 0.002 af

0.03 cfs @ 12.08 hrs, Volume= Outflow 0.002 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Reach R2: Reach 2



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Summary for Pond Lot 3: Roof Recharge

Inflow Area =	0.057 ac,100.00% Impervious, Inflow De	epth > 3.08" for 2-Year event
Inflow =	0.19 cfs @ 12.07 hrs, Volume=	0.015 af
Outflow =	0.02 cfs @ 11.44 hrs, Volume=	0.015 af, Atten= 91%, Lag= 0.0 min
Discarded =	0.02 cfs @ 11.44 hrs, Volume=	0.015 af
Primary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 104.13' @ 12.84 hrs Surf.Area= 0.007 ac Storage= 0.005 af

Plug-Flow detention time= 85.1 min calculated for 0.015 af (100% of inflow) Center-of-Mass det. time= 84.4 min (838.7 - 754.3)

Volume	Invert	Avail.Storage	Storage Description
#1A	103.00'	0.007 af	30.50'W x 10.50'L x 3.54'H Field A
			0.026 af Overall - 0.009 af Embedded = 0.017 af x 40.0% Voids
#2A	103.50'	0.009 af	Cultec R-330XLHD x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		0.016 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	103.00'	2.410 in/hr Exfiltration over Surface area
#2	Primary	108.00'	12.0" Horiz. Orifice/Grate C= 0.600
	-		Limited to weir flow at low heads

Discarded OutFlow Max=0.02 cfs @ 11.44 hrs HW=103.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=103.00' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs)

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Pond Lot 3: Roof Recharge - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

1 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 8.50' Row Length +12.0" End Stone x 2 = 10.50' Base Length

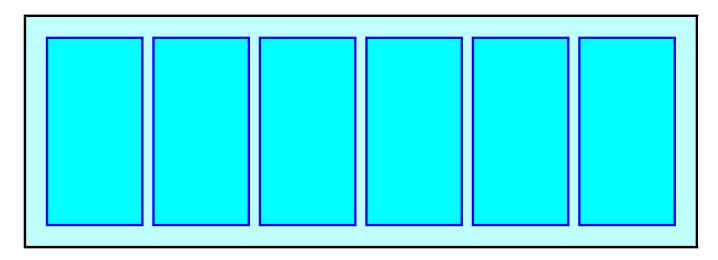
6 Rows x 52.0" Wide + 6.0" Spacing x 5 + 12.0" Side Stone x 2 = 30.50' Base Width 6.0" Stone Base + 30.5" Chamber Height + 6.0" Stone Cover = 3.54' Field Height

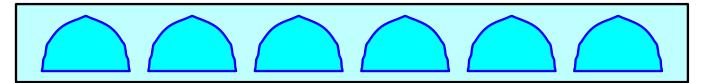
6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 380.0 cf Chamber Storage

1,134.2 cf Field - 380.0 cf Chambers = 754.2 cf Stone x 40.0% Voids = 301.7 cf Stone Storage

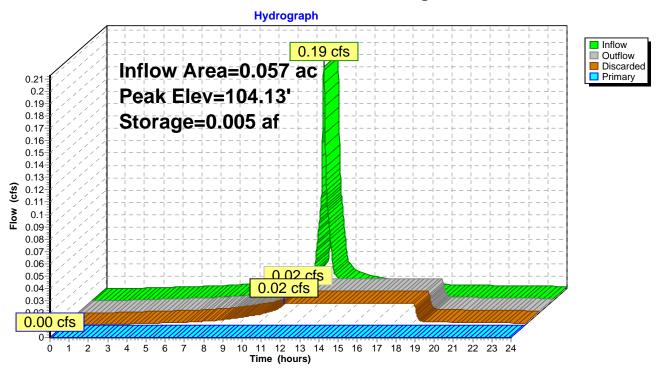
Chamber Storage + Stone Storage = 681.7 cf = 0.016 af Overall Storage Efficiency = 60.1% Overall System Size = 10.50' x 30.50' x 3.54'

6 Chambers 42.0 cy Field 27.9 cy Stone





Pond Lot 3: Roof Recharge



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Summary for Pond Lot 4: Roof Recharge

Inflow Area =	0.057 ac,100.00% Impervious, Inflow De	epth > 3.08" for 2-Year event
Inflow =	0.19 cfs @ 12.07 hrs, Volume=	0.015 af
Outflow =	0.02 cfs @ 11.44 hrs, Volume=	0.015 af, Atten= 91%, Lag= 0.0 min
Discarded =	0.02 cfs @ 11.44 hrs, Volume=	0.015 af
Primary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 104.13' @ 12.84 hrs Surf.Area= 0.007 ac Storage= 0.005 af

Plug-Flow detention time= 85.1 min calculated for 0.015 af (100% of inflow) Center-of-Mass det. time= 84.4 min (838.7 - 754.3)

Volume	Invert	Avail.Storage	Storage Description
#1A	103.00' 0.007 af		30.50'W x 10.50'L x 3.54'H Field A
			0.026 af Overall - 0.009 af Embedded = 0.017 af x 40.0% Voids
#2A	103.50'	0.009 af	Cultec R-330XLHD x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		0.016 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	103.00'	2.410 in/hr Exfiltration over Surface area
#2	Primary	108.00'	12.0" Horiz. Orifice/Grate C= 0.600
			I imited to weir flow at low heads

Discarded OutFlow Max=0.02 cfs @ 11.44 hrs HW=103.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=103.00' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs)

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Pond Lot 4: Roof Recharge - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

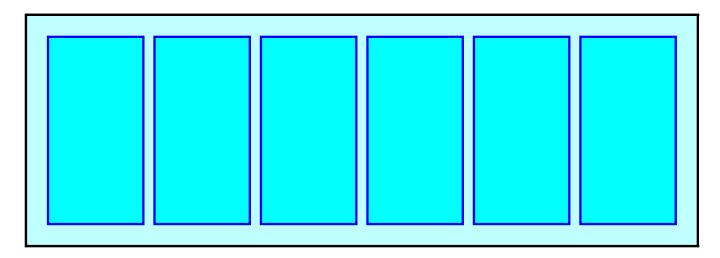
Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

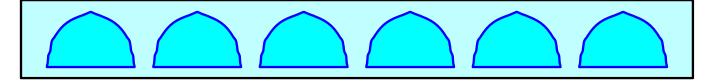
52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

- 1 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 8.50' Row Length +12.0" End Stone x 2 = 10.50' Base Length
- 6 Rows x 52.0" Wide + 6.0" Spacing x 5 + 12.0" Side Stone x 2 = 30.50' Base Width 6.0" Stone Base + 30.5" Chamber Height + 6.0" Stone Cover = 3.54' Field Height
- 6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 380.0 cf Chamber Storage
- 1,134.2 cf Field 380.0 cf Chambers = 754.2 cf Stone x 40.0% Voids = 301.7 cf Stone Storage

Chamber Storage + Stone Storage = 681.7 cf = 0.016 af Overall Storage Efficiency = 60.1% Overall System Size = 10.50' x 30.50' x 3.54'

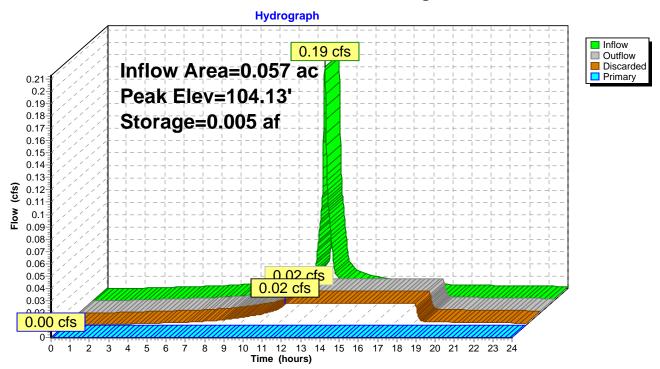
6 Chambers 42.0 cy Field 27.9 cy Stone





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Pond Lot 4: Roof Recharge



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Summary for Pond PR1: Recharge 1

Inflow Area =	1.077 ac, 34.35% Impervious, Inflow Do	epth > 1.55" for 2-Year event
Inflow =	1.63 cfs @ 12.16 hrs, Volume=	0.139 af
Outflow =	0.22 cfs @ 11.81 hrs, Volume=	0.139 af, Atten= 87%, Lag= 0.0 min
Discarded =	0.22 cfs @ 11.81 hrs, Volume=	0.139 af
Primary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 103.92' @ 13.04 hrs Surf.Area= 0.089 ac Storage= 0.050 af

Plug-Flow detention time= 84.3 min calculated for 0.139 af (100% of inflow) Center-of-Mass det. time= 83.4 min (924.8 - 841.4)

Volume	Invert	Avail.Storage	Storage Description
#1A	A 103.00' 0.075 at		74.00'W x 52.50'L x 3.54'H Field A
			0.316 af Overall - 0.130 af Embedded = 0.186 af x 40.0% Voids
#2A	103.50'	0.130 af	Cultec R-330XLHD x 105 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 15 rows
		0.204 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	103.00'	2.410 in/hr Exfiltration over Surface area
#2	Primary	108.00'	12.0" Horiz. Orifice/Grate C= 0.600
			I imited to weir flow at low heads

Discarded OutFlow Max=0.22 cfs @ 11.81 hrs HW=103.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.22 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=103.00' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs)

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Pond PR1: Recharge 1 - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 15 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

7 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 50.50' Row Length +12.0" End Stone x 2 = 52.50' Base Length

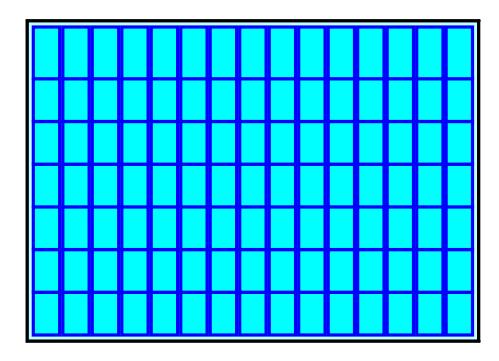
15 Rows x 52.0" Wide + 6.0" Spacing x 14 + 12.0" Side Stone x 2 = 74.00' Base Width 6.0" Stone Base + 30.5" Chamber Height + 6.0" Stone Cover = 3.54' Field Height

105 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 15 Rows = 5,644.1 cf Chamber Storage

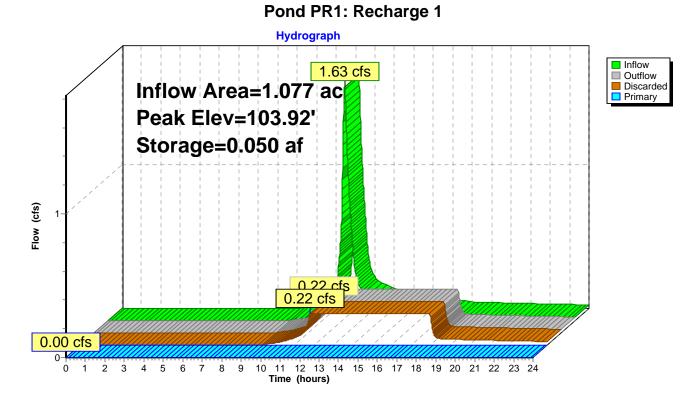
13,759.4 cf Field - 5,644.1 cf Chambers = 8,115.2 cf Stone x 40.0% Voids = 3,246.1 cf Stone Storage

Chamber Storage + Stone Storage = 8,890.2 cf = 0.204 af Overall Storage Efficiency = 64.6% Overall System Size = 52.50' x 74.00' x 3.54'

105 Chambers 509.6 cy Field 300.6 cy Stone







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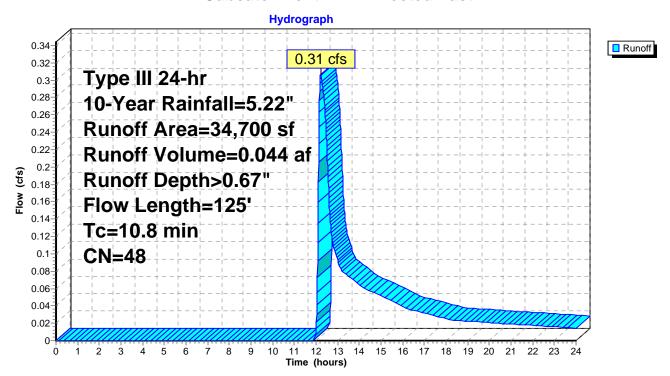
Summary for Subcatchment P1A: Directed East

Runoff = 0.31 cfs @ 12.22 hrs, Volume= 0.044 af, Depth> 0.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.22"

_	Α	rea (sf)	CN	Description				
*		2,854	98	Impervious				
		14,380	39	>75% Gras	s cover, Go	ood, HSG A		
		11,288	30	Woods, Go	od, HSG A			
		3,734	74	>75% Gras	s cover, Go	ood, HSG C		
		111	70	Woods, Go	od, HSG C			
		2,333	80	>75% Gras	s cover, Go	ood, HSG D		
		34,700	48	Weighted A	verage			
		31,846		91.78% Pei	rvious Area			
		2,854		8.22% Impe	ervious Area	a		
				•				
	Tc	Length	Slope	Velocity	Capacity	Description		
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	10.0	50	0.1400	0.08		Sheet Flow, Sheet Flow Woods		
						Woods: Dense underbrush n= 0.800 P2= 3.10"		
	8.0	75	0.1067	1.63		Shallow Concentrated Flow, Concentrated Woods		
_						Woodland Kv= 5.0 fps		
	10.8	125	Total					

Subcatchment P1A: Directed East



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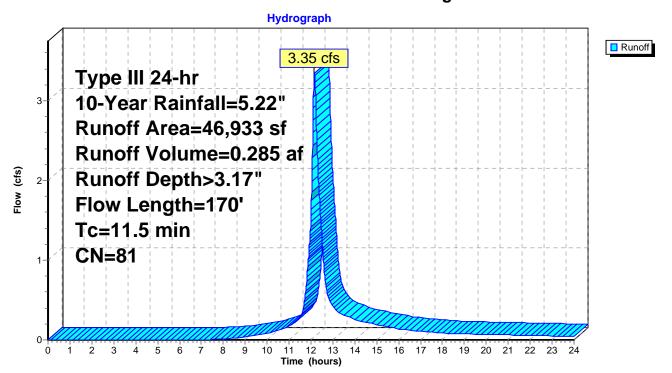
Summary for Subcatchment P1B: To Recharge 1

Runoff = 3.35 cfs @ 12.16 hrs, Volume= 0.285 af, Depth> 3.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.22"

	Α	rea (sf)	CN	Description		
*		16,120	98	Impervious		
		989	39	>75% Gras	s cover, Go	ood, HSG A
		21,312	74	>75% Gras	s cover, Go	ood, HSG C
		8,215	70	Woods, Go	od, HSG C	
_		297	80	>75% Gras	s cover, Go	ood, HSG D
		46,933	81	Weighted A	verage	
		30,813		65.65% Pe	rvious Area	
		16,120	;	34.35% lmp	pervious Ar	ea
	_					
	Tc	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	10.0	50	0.1400	0.08		Sheet Flow, Wood Sheet Flow
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	1.5	120	0.0750	1.37		Shallow Concentrated Flow, Woods Concentrated Flow
_						Woodland Kv= 5.0 fps
	11.5	170	Total			

Subcatchment P1B: To Recharge 1



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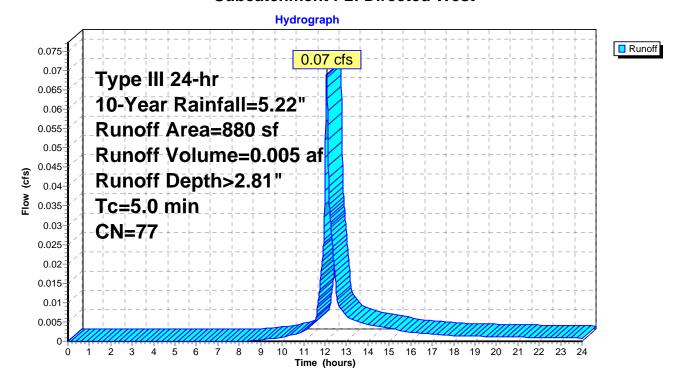
Summary for Subcatchment P2: Directed West

Runoff = 0.07 cfs @ 12.08 hrs, Volume= 0.005 af, Depth> 2.81"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.22"

A	rea (sf)	CN	Description				
	473	74	>75% Gras	s cover, Go	ood, HSG C		
	407	80	>75% Gras	s cover, Go	ood, HSG D		
	880	77	Weighted Average				
	880		100.00% Pervious Area				
т.	l a.a.a.tla	Ola a	Malaait.	0	Description		
Tc	Length	Slope	,	Capacity	Description		
(min)	(feet)	(ft/ft	(ft/sec)	(cfs)			
5.0		_			Direct Entry,		

Subcatchment P2: Directed West



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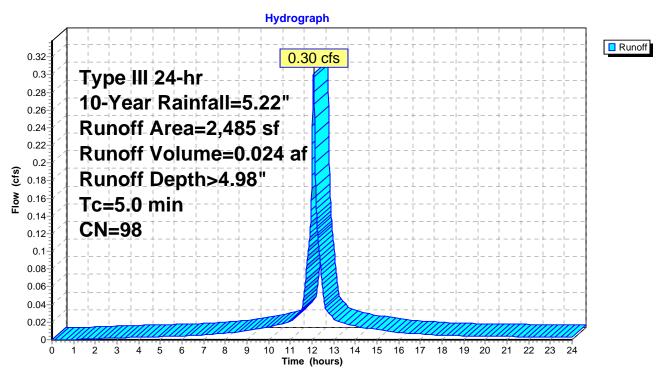
Summary for Subcatchment RR3: Roof Runoff - Lot 3

Runoff = 0.30 cfs @ 12.07 hrs, Volume= 0.024 af, Depth> 4.98"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.22"

	Α	rea (sf)	CN	Description			
*		2,485	98	Roof			
		2,485		100.00% Impervious Area			
	Tc	Length	Slope	Velocity	Capacity	Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	5.0					Direct Entry,	

Subcatchment RR3: Roof Runoff - Lot 3



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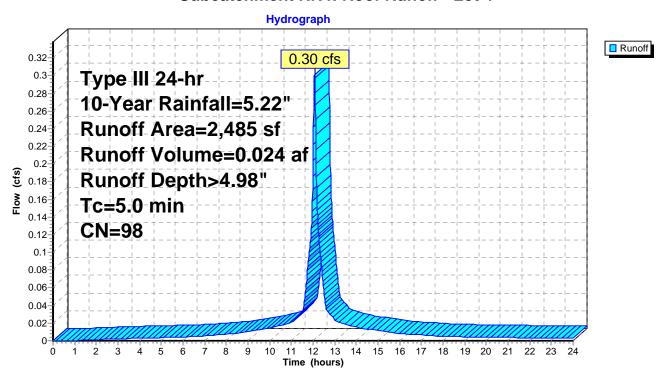
Summary for Subcatchment RR4: Roof Runoff - Lot 4

Runoff = 0.30 cfs @ 12.07 hrs, Volume= 0.024 af, Depth> 4.98"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.22"

	Α	rea (sf)	CN	Description		
*		2,485	98	Roof		
		2,485		100.00% In	Area	
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·
	5.0					Direct Entry,

Subcatchment RR4: Roof Runoff - Lot 4



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Summary for Reach P: Total

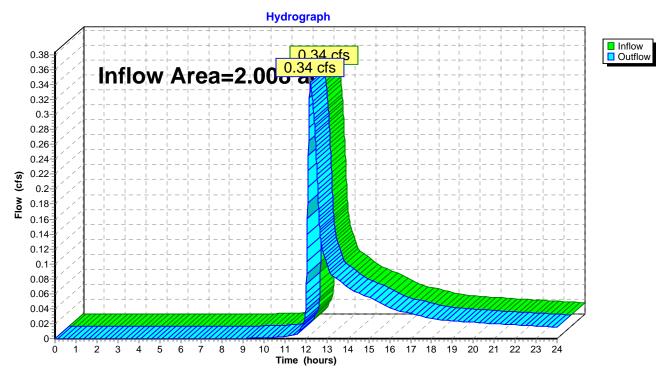
Inflow Area = 2.008 ac, 27.37% Impervious, Inflow Depth > 0.29" for 10-Year event

0.34 cfs @ 12.21 hrs, Volume= Inflow 0.049 af

0.34 cfs @ 12.21 hrs, Volume= Outflow 0.049 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Reach P: Total



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Summary for Reach R1: Reach 1

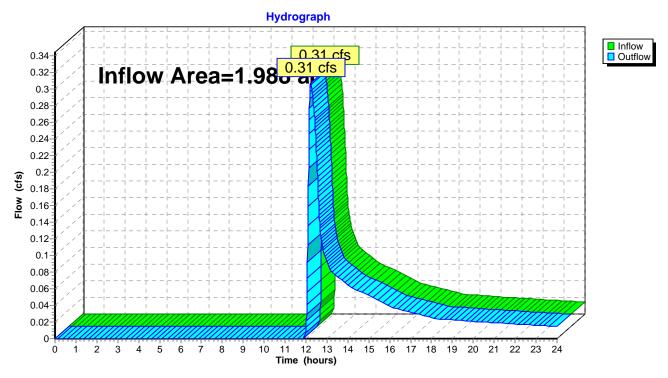
1.988 ac, 27.65% Impervious, Inflow Depth > 0.27" for 10-Year event Inflow Area =

0.31 cfs @ 12.22 hrs, Volume= Inflow 0.044 af

0.31 cfs @ 12.22 hrs, Volume= Outflow 0.044 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Reach R1: Reach 1



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Summary for Reach R2: Reach 2

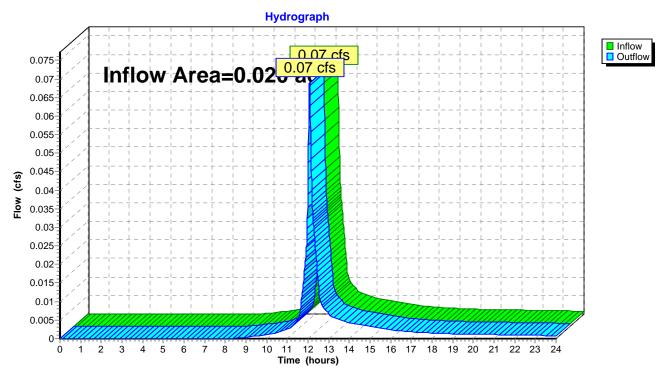
Inflow Area = 0.00% Impervious, Inflow Depth > 2.81" for 10-Year event

0.07 cfs @ 12.08 hrs, Volume= Inflow 0.005 af

0.07 cfs @ 12.08 hrs, Volume= Outflow 0.005 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Reach R2: Reach 2



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Summary for Pond Lot 3: Roof Recharge

Inflow Area =	0.057 ac,100.00% Impervious, Inflow Do	epth > 4.98" for 10-Year event
Inflow =	0.30 cfs @ 12.07 hrs, Volume=	0.024 af
Outflow =	0.02 cfs @ 10.68 hrs, Volume=	0.024 af, Atten= 94%, Lag= 0.0 min
Discarded =	0.02 cfs @ 10.68 hrs, Volume=	0.024 af
Primary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 104.99' @ 13.63 hrs Surf.Area= 0.007 ac Storage= 0.010 af

Plug-Flow detention time= 184.2 min calculated for 0.024 af (100% of inflow)

Center-of-Mass det. time= 183.5 min (929.4 - 745.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	103.00'	0.007 af	30.50'W x 10.50'L x 3.54'H Field A
			0.026 af Overall - 0.009 af Embedded = 0.017 af x 40.0% Voids
#2A	103.50'	0.009 af	Cultec R-330XLHD x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		0.016 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	103.00'	2.410 in/hr Exfiltration over Surface area
#2	Primary	108.00'	12.0" Horiz. Orifice/Grate C= 0.600
			I imited to weir flow at low heads

Discarded OutFlow Max=0.02 cfs @ 10.68 hrs HW=103.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=103.00' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs)

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Pond Lot 3: Roof Recharge - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

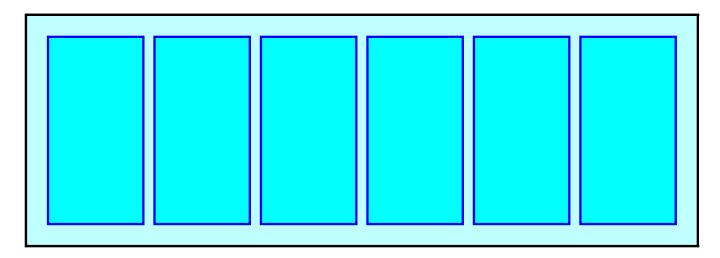
Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

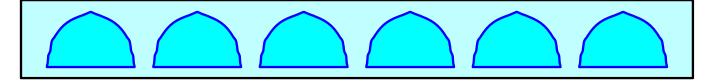
52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

- 1 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 8.50' Row Length +12.0" End Stone x 2 = 10.50' Base Length
- 6 Rows x 52.0" Wide + 6.0" Spacing x 5 + 12.0" Side Stone x 2 = 30.50' Base Width 6.0" Stone Base + 30.5" Chamber Height + 6.0" Stone Cover = 3.54' Field Height
- 6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 380.0 cf Chamber Storage
- 1,134.2 cf Field 380.0 cf Chambers = 754.2 cf Stone x 40.0% Voids = 301.7 cf Stone Storage

Chamber Storage + Stone Storage = 681.7 cf = 0.016 af Overall Storage Efficiency = 60.1% Overall System Size = 10.50' x 30.50' x 3.54'

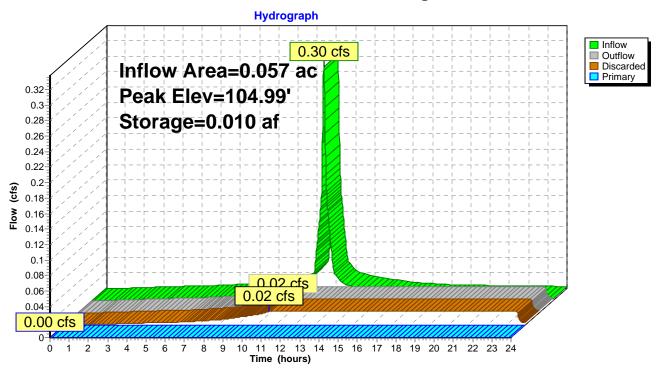
6 Chambers 42.0 cy Field 27.9 cy Stone





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Pond Lot 3: Roof Recharge



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Summary for Pond Lot 4: Roof Recharge

Inflow Area =	0.057 ac,100.00% Impervious, Inflow Do	epth > 4.98" for 10-Year event
Inflow =	0.30 cfs @ 12.07 hrs, Volume=	0.024 af
Outflow =	0.02 cfs @ 10.68 hrs, Volume=	0.024 af, Atten= 94%, Lag= 0.0 min
Discarded =	0.02 cfs @ 10.68 hrs, Volume=	0.024 af
Primary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 104.99' @ 13.63 hrs Surf.Area= 0.007 ac Storage= 0.010 af

Plug-Flow detention time= 184.2 min calculated for 0.024 af (100% of inflow)

Center-of-Mass det. time= 183.5 min (929.4 - 745.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	103.00'	0.007 af	30.50'W x 10.50'L x 3.54'H Field A
			0.026 af Overall - 0.009 af Embedded = 0.017 af x 40.0% Voids
#2A	103.50'	0.009 af	Cultec R-330XLHD x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		0.016 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	103.00'	2.410 in/hr Exfiltration over Surface area
#2	Primary	108.00'	12.0" Horiz. Orifice/Grate C= 0.600
	•		I imited to weir flow at low heads

Discarded OutFlow Max=0.02 cfs @ 10.68 hrs HW=103.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=103.00' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs)

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Pond Lot 4: Roof Recharge - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

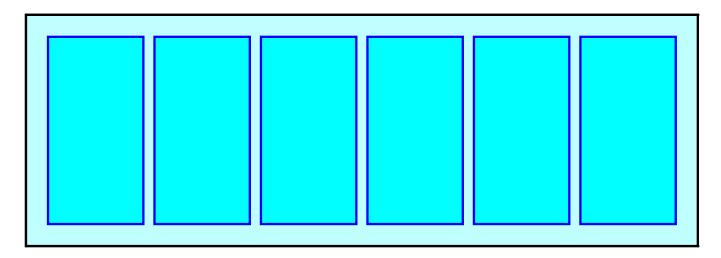
Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

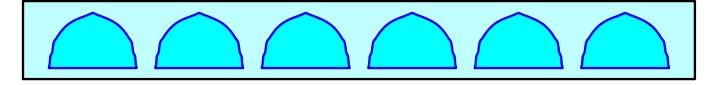
52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

- 1 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 8.50' Row Length +12.0" End Stone x 2 = 10.50' Base Length
- 6 Rows x 52.0" Wide + 6.0" Spacing x 5 + 12.0" Side Stone x 2 = 30.50' Base Width 6.0" Stone Base + 30.5" Chamber Height + 6.0" Stone Cover = 3.54' Field Height
- 6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 380.0 cf Chamber Storage
- 1,134.2 cf Field 380.0 cf Chambers = 754.2 cf Stone x 40.0% Voids = 301.7 cf Stone Storage

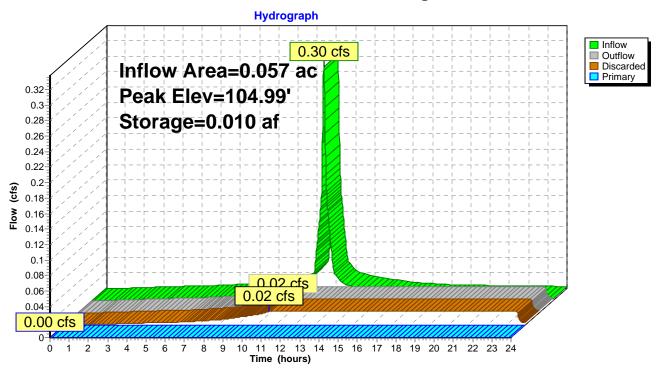
Chamber Storage + Stone Storage = 681.7 cf = 0.016 af Overall Storage Efficiency = 60.1% Overall System Size = 10.50' x 30.50' x 3.54'

6 Chambers 42.0 cy Field 27.9 cy Stone





Pond Lot 4: Roof Recharge



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Summary for Pond PR1: Recharge 1

Inflow Area = 1.077 ac, 34.35% Impervious, Inflow Depth > 3.17" for 10-Year event
Inflow = 3.35 cfs @ 12.16 hrs, Volume= 0.285 af
Outflow = 0.22 cfs @ 11.36 hrs, Volume= 0.248 af, Atten= 94%, Lag= 0.0 min
Discarded = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 105.12' @ 14.56 hrs Surf.Area= 0.089 ac Storage= 0.137 af

Plug-Flow detention time= 260.0 min calculated for 0.248 af (87% of inflow) Center-of-Mass det. time= 202.0 min (1,023.0 - 821.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	103.00'	0.075 af	74.00'W x 52.50'L x 3.54'H Field A
			0.316 af Overall - 0.130 af Embedded = 0.186 af x 40.0% Voids
#2A	103.50'	0.130 af	Cultec R-330XLHD x 105 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 15 rows
		0.204 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	103.00'	2.410 in/hr Exfiltration over Surface area
#2	Primary	108.00'	12.0" Horiz. Orifice/Grate C= 0.600
			I imited to weir flow at low heads

Discarded OutFlow Max=0.22 cfs @ 11.36 hrs HW=103.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.22 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=103.00' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs)

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Pond PR1: Recharge 1 - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 15 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

7 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 50.50' Row Length +12.0" End Stone x 2 = 52.50' Base Length

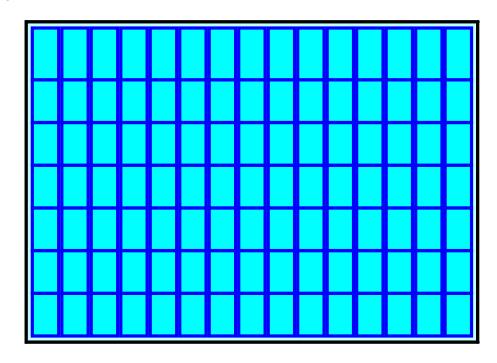
15 Rows x 52.0" Wide + 6.0" Spacing x 14 + 12.0" Side Stone x 2 = 74.00' Base Width 6.0" Stone Base + 30.5" Chamber Height + 6.0" Stone Cover = 3.54' Field Height

105 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 15 Rows = 5,644.1 cf Chamber Storage

13,759.4 cf Field - 5,644.1 cf Chambers = 8,115.2 cf Stone x 40.0% Voids = 3,246.1 cf Stone Storage

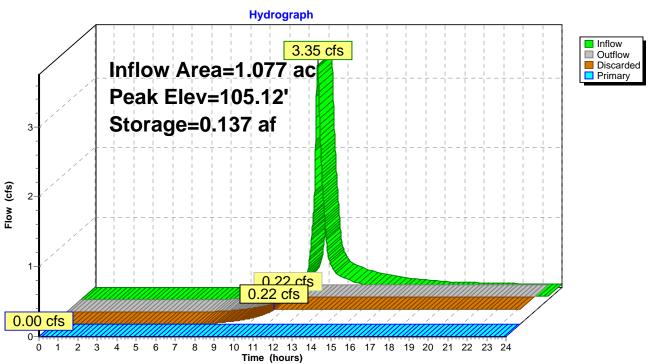
Chamber Storage + Stone Storage = 8,890.2 cf = 0.204 af Overall Storage Efficiency = 64.6% Overall System Size = 52.50' x 74.00' x 3.54'

105 Chambers 509.6 cy Field 300.6 cy Stone





Pond PR1: Recharge 1



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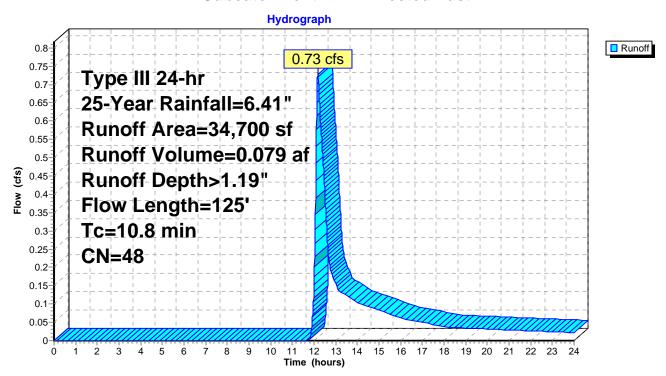
Summary for Subcatchment P1A: Directed East

Runoff 0.73 cfs @ 12.18 hrs, Volume= 0.079 af, Depth> 1.19"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

	Α	rea (sf)	CN	Description				
*		2,854	98	Impervious				
		14,380	39	>75% Gras	s cover, Go	ood, HSG A		
		11,288	30	Woods, Go	od, HSG A			
		3,734	74	>75% Gras	s cover, Go	ood, HSG C		
		111	70	Woods, Good, HSG C				
_		2,333	80	>75% Gras	s cover, Go	ood, HSG D		
34,700 48 Weighted Average								
		31,846		91.78% Pei	rvious Area			
		2,854		8.22% Impe	ervious Area	a		
				•				
	Tc	Length	Slope	Velocity	Capacity	Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
_	10.0	50	0.1400	0.08		Sheet Flow, Sheet Flow Woods		
						Woods: Dense underbrush n= 0.800 P2= 3.10"		
	8.0	75	0.1067	1.63		Shallow Concentrated Flow, Concentrated Woods		
_						Woodland Kv= 5.0 fps		
	10.8	125	Total	_	_			

Subcatchment P1A: Directed East



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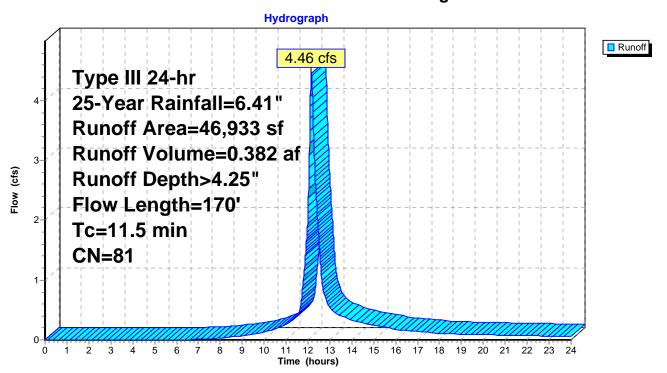
Summary for Subcatchment P1B: To Recharge 1

Runoff 4.46 cfs @ 12.16 hrs, Volume= 0.382 af, Depth> 4.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

	Δ	rea (sf)	CN	Description		
*		16,120	98	Impervious		
		989	39	>75% Gras	s cover, Go	ood, HSG A
		21,312	74	>75% Gras	s cover, Go	ood, HSG C
		8,215	70	Woods, Go	od, HSG C	
		297	80	>75% Gras	s cover, Go	ood, HSG D
		46,933	81	Weighted A	verage	
		30,813		65.65% Pe	rvious Area	
		16,120		34.35% lm _l	pervious Ar	ea
	_					
	Tc	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	10.0	50	0.1400	0.08		Sheet Flow, Wood Sheet Flow
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	1.5	120	0.0750	1.37		Shallow Concentrated Flow, Woods Concentrated Flow
_						Woodland Kv= 5.0 fps
	11.5	170	Total			

Subcatchment P1B: To Recharge 1



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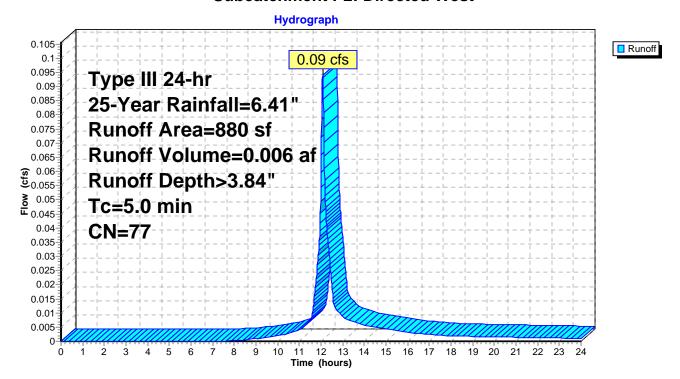
Summary for Subcatchment P2: Directed West

Runoff = 0.09 cfs @ 12.07 hrs, Volume= 0.006 af, Depth> 3.84"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

A	rea (sf)	CN	Description		
	473	74	>75% Gras	s cover, Go	ood, HSG C
	407	80	>75% Gras	s cover, Go	ood, HSG D
	880	77	Weighted A	verage	
	880		100.00% Pe	ervious Are	ea
т.	l a.a.a.tla	Ola a	Malaait.	0	Description
Tc	Length	Slope	,	Capacity	Description
(min)	(feet)	(ft/ft	(ft/sec)	(cfs)	
5.0		_			Direct Entry,

Subcatchment P2: Directed West



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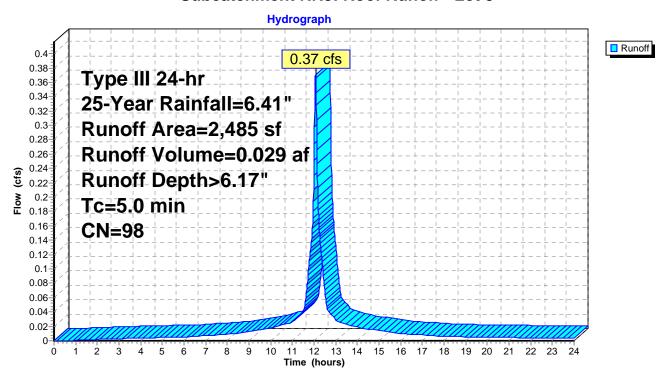
Summary for Subcatchment RR3: Roof Runoff - Lot 3

Runoff = 0.37 cfs @ 12.07 hrs, Volume= 0.029 af, Depth> 6.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

	Α	rea (sf)	CN	Description			
*		2,485	98	Roof			
		2,485		100.00% Impervious Area			
	Tc	Length	Slope	Velocity	Capacity	Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·	
	5.0					Direct Entry,	

Subcatchment RR3: Roof Runoff - Lot 3



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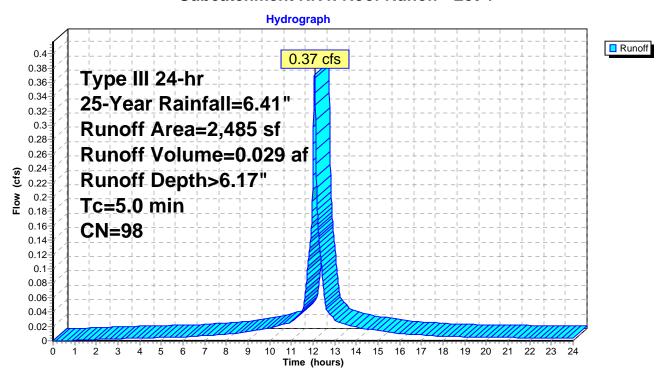
Summary for Subcatchment RR4: Roof Runoff - Lot 4

Runoff = 0.37 cfs @ 12.07 hrs, Volume= 0.029 af, Depth> 6.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

	Α	rea (sf)	CN	Description			
*		2,485	98	Roof			
		2,485		100.00% Impervious Area			
	Tc	Length	Slope	Velocity	Capacity	Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·	
	5.0					Direct Entry,	

Subcatchment RR4: Roof Runoff - Lot 4



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Summary for Reach P: Total

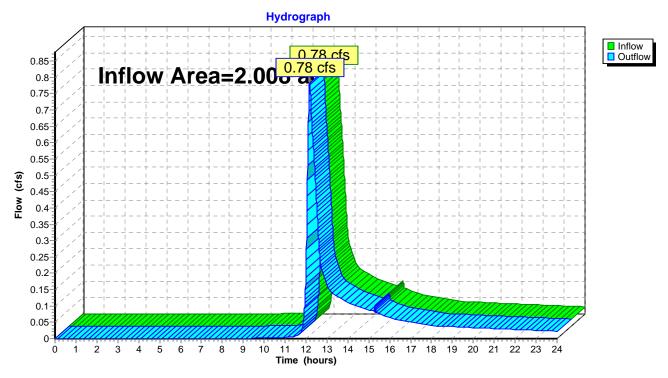
Inflow Area = 2.008 ac, 27.37% Impervious, Inflow Depth > 0.51" for 25-Year event

0.78 cfs @ 12.18 hrs, Volume= Inflow 0.086 af

0.78 cfs @ 12.18 hrs, Volume= Outflow 0.086 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Reach P: Total



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Summary for Reach R1: Reach 1

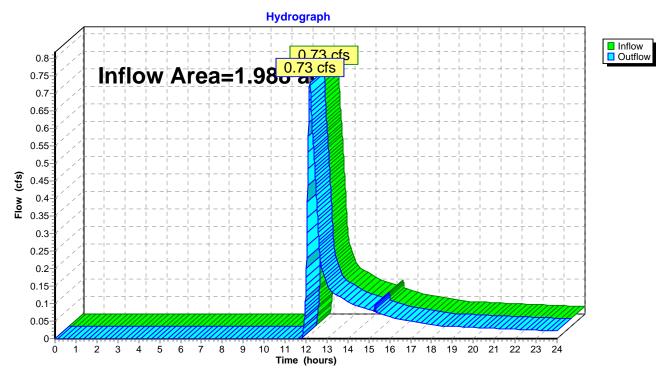
Inflow Area = 1.988 ac, 27.65% Impervious, Inflow Depth > 0.48" for 25-Year event

0.73 cfs @ 12.18 hrs, Volume= Inflow 0.079 af

0.73 cfs @ 12.18 hrs, Volume= Outflow 0.079 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Reach R1: Reach 1



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Summary for Reach R2: Reach 2

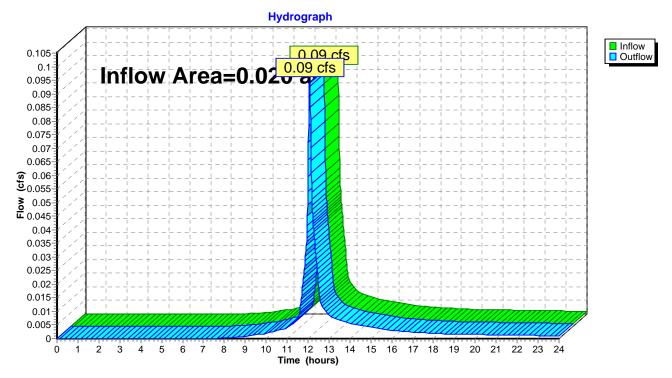
Inflow Area = 0.020 ac, 0.00% Impervious, Inflow Depth > 3.84" for 25-Year event

Inflow = 0.09 cfs @ 12.07 hrs, Volume= 0.006 af

Outflow = 0.09 cfs @ 12.07 hrs, Volume= 0.006 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Reach R2: Reach 2



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Summary for Pond Lot 3: Roof Recharge

Inflow Area =	0.057 ac,100.00% Impervious, Inflow Do	epth > 6.17" for 25-Year event
Inflow =	0.37 cfs @ 12.07 hrs, Volume=	0.029 af
Outflow =	0.02 cfs @ 10.18 hrs, Volume=	0.025 af, Atten= 95%, Lag= 0.0 min
Discarded =	0.02 cfs @ 10.18 hrs, Volume=	0.025 af
Primary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 105.72' @ 14.12 hrs Surf.Area= 0.007 ac Storage= 0.013 af

Plug-Flow detention time= 235.3 min calculated for 0.025 af (86% of inflow) Center-of-Mass det. time= 172.4 min (915.2 - 742.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	103.00'	0.007 af	30.50'W x 10.50'L x 3.54'H Field A
			0.026 af Overall - 0.009 af Embedded = 0.017 af x 40.0% Voids
#2A	103.50'	0.009 af	Cultec R-330XLHD x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		0.016 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	103.00'	2.410 in/hr Exfiltration over Surface area
#2	Primary	108.00'	12.0" Horiz. Orifice/Grate C= 0.600
	•		I imited to weir flow at low heads

Discarded OutFlow Max=0.02 cfs @ 10.18 hrs HW=103.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=103.00' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs)

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Pond Lot 3: Roof Recharge - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

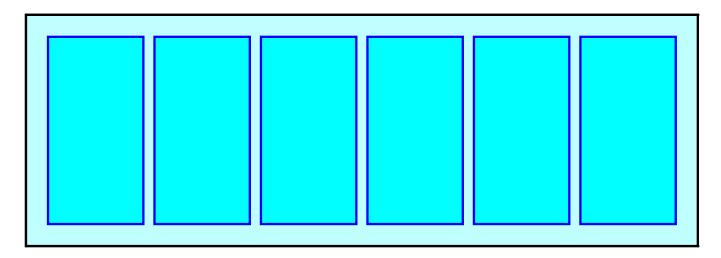
Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

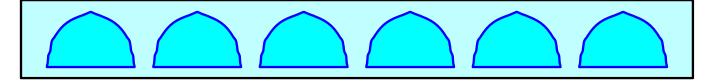
52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

- 1 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 8.50' Row Length +12.0" End Stone x 2 = 10.50' Base Length
- 6 Rows x 52.0" Wide + 6.0" Spacing x 5 + 12.0" Side Stone x 2 = 30.50' Base Width 6.0" Stone Base + 30.5" Chamber Height + 6.0" Stone Cover = 3.54' Field Height
- 6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 380.0 cf Chamber Storage
- 1,134.2 cf Field 380.0 cf Chambers = 754.2 cf Stone x 40.0% Voids = 301.7 cf Stone Storage

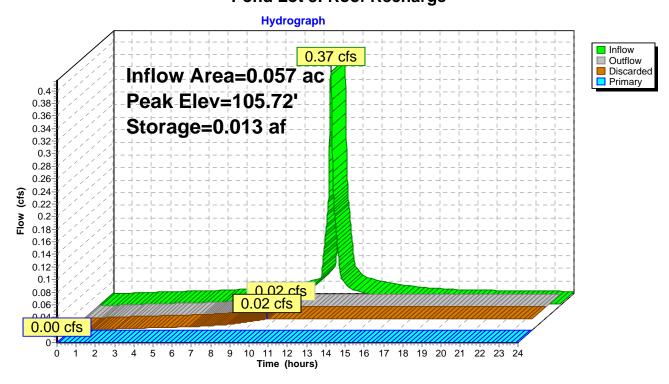
Chamber Storage + Stone Storage = 681.7 cf = 0.016 af Overall Storage Efficiency = 60.1% Overall System Size = 10.50' x 30.50' x 3.54'

6 Chambers 42.0 cy Field 27.9 cy Stone





Pond Lot 3: Roof Recharge



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Summary for Pond Lot 4: Roof Recharge

Inflow Area =	0.057 ac,100.00% Impervious, Inflow De	epth > 6.17" for 25-Year event
Inflow =	0.37 cfs @ 12.07 hrs, Volume=	0.029 af
Outflow =	0.02 cfs @ 10.18 hrs, Volume=	0.025 af, Atten= 95%, Lag= 0.0 min
Discarded =	0.02 cfs @ 10.18 hrs, Volume=	0.025 af
Primary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 105.72' @ 14.12 hrs Surf.Area= 0.007 ac Storage= 0.013 af

Plug-Flow detention time= 235.3 min calculated for 0.025 af (86% of inflow) Center-of-Mass det. time= 172.4 min (915.2 - 742.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	103.00'	0.007 af	30.50'W x 10.50'L x 3.54'H Field A
			0.026 af Overall - 0.009 af Embedded = 0.017 af x 40.0% Voids
#2A	103.50'	0.009 af	Cultec R-330XLHD x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		0.016 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	103.00'	2.410 in/hr Exfiltration over Surface area
#2	Primary	108.00'	12.0" Horiz. Orifice/Grate C= 0.600
	•		I imited to weir flow at low heads

Discarded OutFlow Max=0.02 cfs @ 10.18 hrs HW=103.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=103.00' (Free Discharge) 2=Orifice/Grate (Controls 0.00 cfs)

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Pond Lot 4: Roof Recharge - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

1 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 8.50' Row Length +12.0" End Stone x 2 = 10.50' Base Length

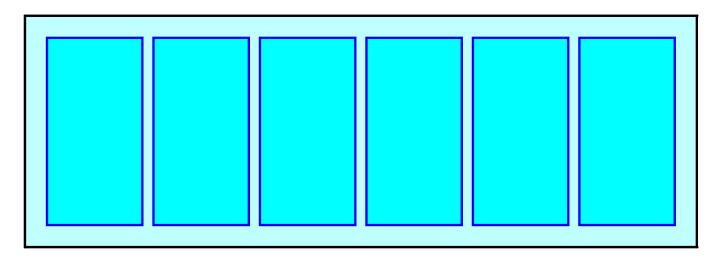
6 Rows x 52.0" Wide + 6.0" Spacing x 5 + 12.0" Side Stone x 2 = 30.50' Base Width 6.0" Stone Base + 30.5" Chamber Height + 6.0" Stone Cover = 3.54' Field Height

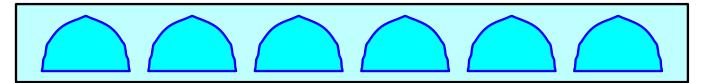
6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 380.0 cf Chamber Storage

1,134.2 cf Field - 380.0 cf Chambers = 754.2 cf Stone x 40.0% Voids = 301.7 cf Stone Storage

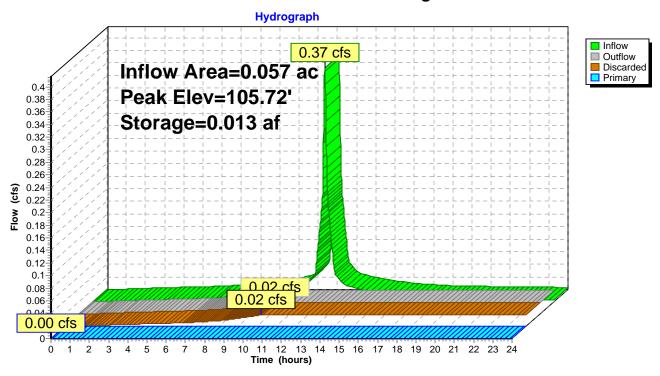
Chamber Storage + Stone Storage = 681.7 cf = 0.016 af Overall Storage Efficiency = 60.1% Overall System Size = 10.50' x 30.50' x 3.54'

6 Chambers 42.0 cy Field 27.9 cy Stone





Pond Lot 4: Roof Recharge



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Summary for Pond PR1: Recharge 1

Inflow Area = 1.077 ac, 34.35% Impervious, Inflow Depth > 4.25" for 25-Year event Inflow = 4.46 cfs @ 12.16 hrs, Volume= 0.382 af Outflow = 0.24 cfs @ 15.26 hrs, Volume= 0.260 af, Atten= 95%, Lag= 186.3 min Discarded = 0.02 cfs @ 10.86 hrs, Volume= 0.260 af Primary = 0.002 cfs @ 15.26 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 108.01' @ 15.26 hrs Surf.Area= 0.089 ac Storage= 0.204 af

Plug-Flow detention time= 284.0 min calculated for 0.260 af (68% of inflow) Center-of-Mass det. time= 189.1 min (1,001.8 - 812.7)

Volume	Invert	Avail.Storage	Storage Description
#1A	103.00'	0.075 af	74.00'W x 52.50'L x 3.54'H Field A
			0.316 af Overall - 0.130 af Embedded = 0.186 af x 40.0% Voids
#2A	103.50'	0.130 af	Cultec R-330XLHD x 105 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 15 rows
		0.204 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	103.00'	2.410 in/hr Exfiltration over Surface area
#2	Primary	108.00'	12.0" Horiz. Orifice/Grate C= 0.600
	•		I imited to weir flow at low heads

Discarded OutFlow Max=0.22 cfs @ 10.86 hrs HW=103.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.22 cfs)

Primary OutFlow Max=0.01 cfs @ 15.26 hrs HW=108.01' (Free Discharge) 2=Orifice/Grate (Weir Controls 0.01 cfs @ 0.32 fps)

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Pond PR1: Recharge 1 - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 15 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

7 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 50.50' Row Length +12.0" End Stone x 2 = 52.50' Base Length

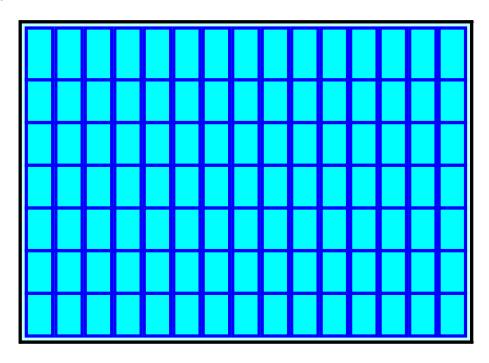
15 Rows x 52.0" Wide + 6.0" Spacing x 14 + 12.0" Side Stone x 2 = 74.00' Base Width 6.0" Stone Base + 30.5" Chamber Height + 6.0" Stone Cover = 3.54' Field Height

105 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 15 Rows = 5,644.1 cf Chamber Storage

13,759.4 cf Field - 5,644.1 cf Chambers = 8,115.2 cf Stone x 40.0% Voids = 3,246.1 cf Stone Storage

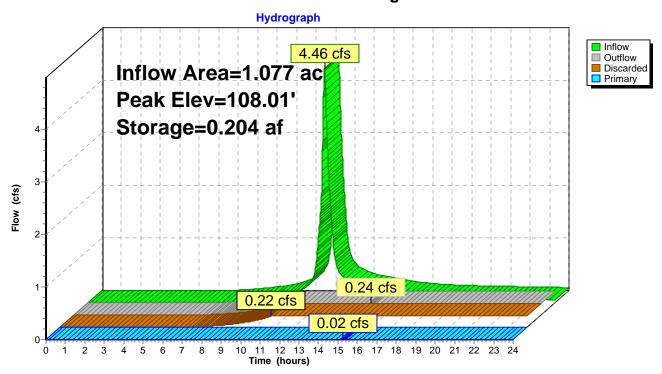
Chamber Storage + Stone Storage = 8,890.2 cf = 0.204 af Overall Storage Efficiency = 64.6% Overall System Size = 52.50' x 74.00' x 3.54'

105 Chambers 509.6 cy Field 300.6 cy Stone





Pond PR1: Recharge 1



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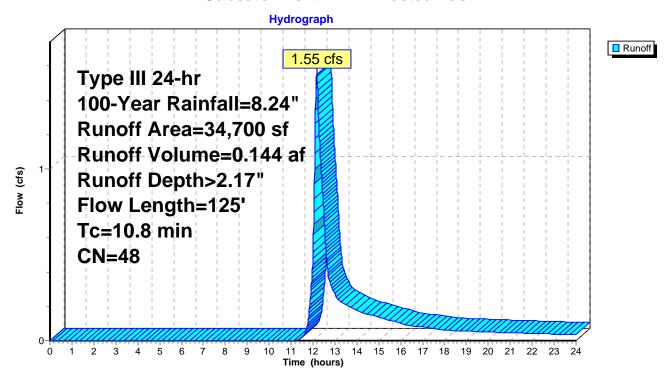
Summary for Subcatchment P1A: Directed East

Runoff = 1.55 cfs @ 12.16 hrs, Volume= 0.144 af, Depth> 2.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=8.24"

	Α	rea (sf)	CN	Description				
*		2,854	98	Impervious				
		14,380	39	>75% Gras	s cover, Go	ood, HSG A		
		11,288	30	Woods, Go	od, HSG A			
		3,734	74	>75% Gras	s cover, Go	ood, HSG C		
		111	70	Woods, Go	od, HSG C			
_		2,333	80	>75% Gras	s cover, Go	ood, HSG D		
		34,700	48	Weighted A	verage			
		31,846		91.78% Pei	rvious Area			
		2,854		8.22% Impe	ervious Area	a		
				•				
	Tc	Length	Slope	Velocity	Capacity	Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
_	10.0	50	0.1400	0.08		Sheet Flow, Sheet Flow Woods		
						Woods: Dense underbrush n= 0.800 P2= 3.10"		
	8.0	75	0.1067	1.63		Shallow Concentrated Flow, Concentrated Woods		
_						Woodland Kv= 5.0 fps		
	10.8	125	Total	_	_			

Subcatchment P1A: Directed East



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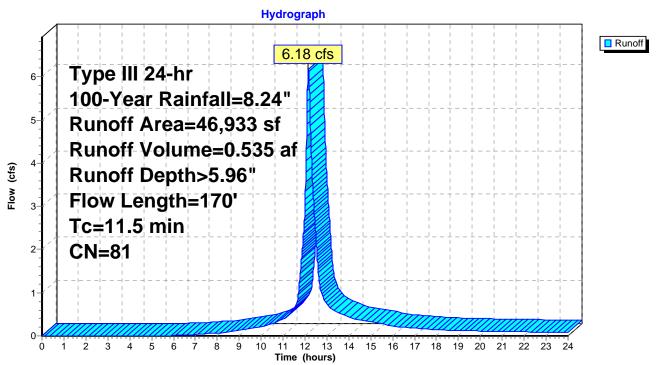
Summary for Subcatchment P1B: To Recharge 1

Runoff 6.18 cfs @ 12.15 hrs, Volume= 0.535 af, Depth> 5.96"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=8.24"

	Δ	rea (sf)	CN	Description			
*		16,120	98	Impervious			
		989	39	>75% Gras	s cover, Go	ood, HSG A	
		21,312	74	>75% Gras	s cover, Go	ood, HSG C	
		8,215	70	Woods, Go	od, HSG C		
		297	80	>75% Gras	s cover, Go	ood, HSG D	
46,933 81 Weighted Average							
		30,813		65.65% Pe	rvious Area		
		16,120		34.35% lm _l	pervious Ar	ea	
	_						
	Tc	Length	Slope		Capacity	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	10.0	50	0.1400	0.08		Sheet Flow, Wood Sheet Flow	
						Woods: Dense underbrush n= 0.800 P2= 3.10"	
	1.5	120	0.0750	1.37		Shallow Concentrated Flow, Woods Concentrated Flow	
_						Woodland Kv= 5.0 fps	
	11.5	170	Total				

Subcatchment P1B: To Recharge 1



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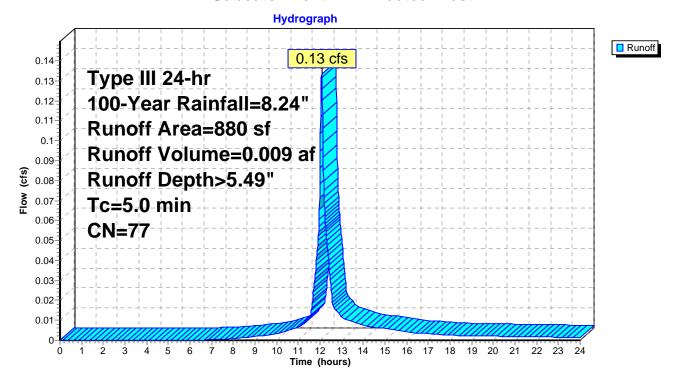
Summary for Subcatchment P2: Directed West

Runoff = 0.13 cfs @ 12.07 hrs, Volume= 0.009 af, Depth> 5.49"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=8.24"

A	rea (sf)	CN	Description					
	473	74	>75% Grass cover, Good, HSG C					
	407	80	>75% Gras	>75% Grass cover, Good, HSG D				
	880	77	Weighted Average					
	880		100.00% Pervious Area					
Tc	Length	Slope	,	Capacity	Description			
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)				
5.0					Direct Entry,			

Subcatchment P2: Directed West



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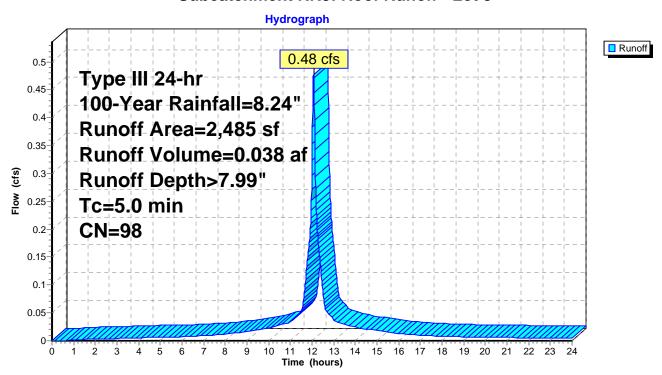
Summary for Subcatchment RR3: Roof Runoff - Lot 3

Runoff = 0.48 cfs @ 12.07 hrs, Volume= 0.038 af, Depth> 7.99"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=8.24"

	Α	rea (sf)	CN	Description					
*		2,485	98	Roof					
		2,485		100.00% Impervious Area					
	Tc	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·			
	5.0					Direct Entry,			

Subcatchment RR3: Roof Runoff - Lot 3



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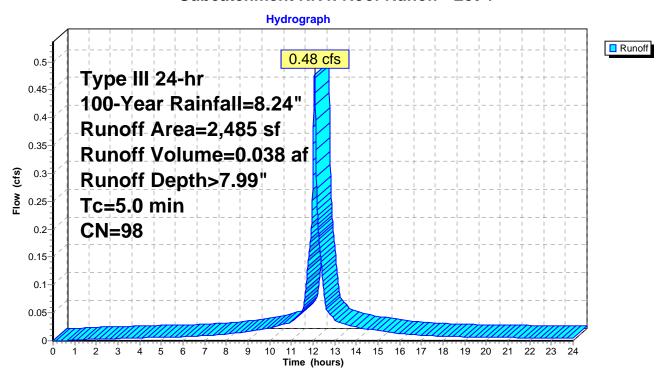
Summary for Subcatchment RR4: Roof Runoff - Lot 4

Runoff = 0.48 cfs @ 12.07 hrs, Volume= 0.038 af, Depth> 7.99"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100-Year Rainfall=8.24"

	Α	rea (sf)	CN	Description					
*		2,485	98	Roof					
		2,485		100.00% Impervious Area					
	Tc	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·			
	5.0					Direct Entry,			

Subcatchment RR4: Roof Runoff - Lot 4



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Summary for Reach P: Total

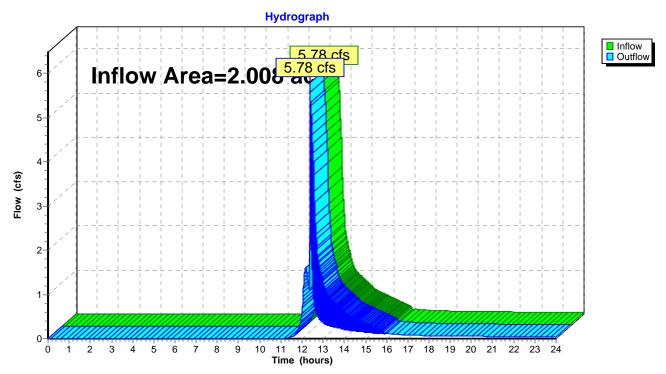
2.008 ac, 27.37% Impervious, Inflow Depth > 1.65" for 100-Year event Inflow Area =

5.78 cfs @ 12.37 hrs, Volume= Inflow 0.276 af

5.78 cfs @ 12.37 hrs, Volume= Outflow 0.276 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Reach P: Total



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Summary for Reach R1: Reach 1

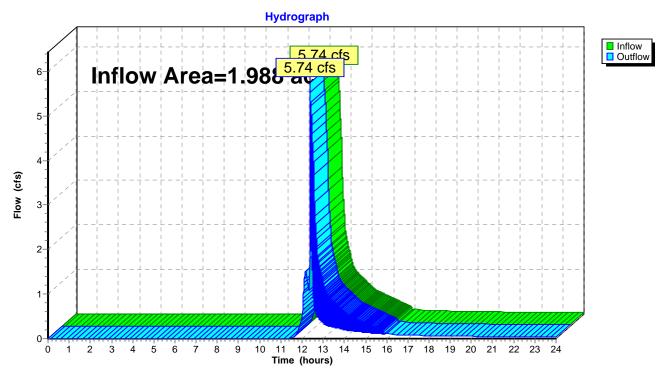
1.988 ac, 27.65% Impervious, Inflow Depth > 1.61" for 100-Year event Inflow Area =

5.74 cfs @ 12.37 hrs, Volume= Inflow 0.267 af

5.74 cfs @ 12.37 hrs, Volume= Outflow 0.267 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Reach R1: Reach 1



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Summary for Reach R2: Reach 2

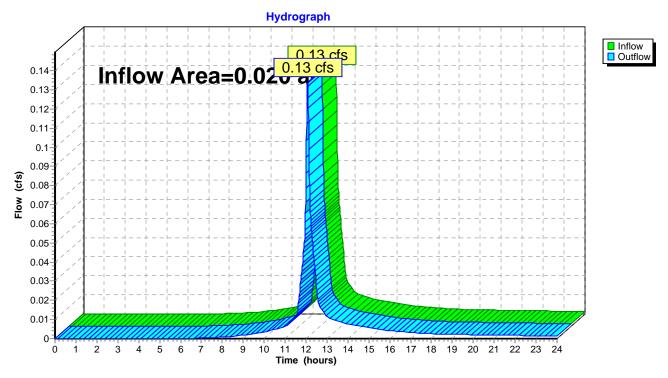
Inflow Area = 0.020 ac, 0.00% Impervious, Inflow Depth > 5.49" for 100-Year event

Inflow = 0.13 cfs @ 12.07 hrs, Volume= 0.009 af

Outflow = 0.13 cfs @ 12.07 hrs, Volume= 0.009 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Reach R2: Reach 2



Type III 24-hr 100-Year Rainfall=8.24"

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Summary for Pond Lot 3: Roof Recharge

Inflow Area =	0.057 ac,100.00% Impervious, Inflow D	epth > 7.99" for 100-Year event
Inflow =	0.48 cfs @ 12.07 hrs, Volume=	0.038 af
Outflow =	0.16 cfs @ 12.42 hrs, Volume=	0.030 af, Atten= 67%, Lag= 21.1 min
Discarded =	0.02 cfs @ 9.27 hrs, Volume=	0.027 af
Primary =	0.14 cfs @ 12.42 hrs, Volume=	0.003 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 108.06' @ 12.42 hrs Surf.Area= 0.007 ac Storage= 0.016 af

Plug-Flow detention time= 216.4 min calculated for 0.030 af (79% of inflow) Center-of-Mass det. time= 135.8 min (875.3 - 739.5)

Volume	Invert	Avail.Storage	Storage Description
#1A	103.00'	0.007 af	30.50'W x 10.50'L x 3.54'H Field A
			0.026 af Overall - 0.009 af Embedded = 0.017 af x 40.0% Voids
#2A	103.50'	0.009 af	Cultec R-330XLHD x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		0.016 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	103.00'	2.410 in/hr Exfiltration over Surface area
#2	Primary	108.00'	12.0" Horiz. Orifice/Grate C= 0.600
	•		I imited to weir flow at low heads

Discarded OutFlow Max=0.02 cfs @ 9.27 hrs HW=103.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=0.12 cfs @ 12.42 hrs HW=108.05' (Free Discharge) 2=Orifice/Grate (Weir Controls 0.12 cfs @ 0.74 fps)

2024-05-10_POST-DRAINAGE

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Pond Lot 3: Roof Recharge - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

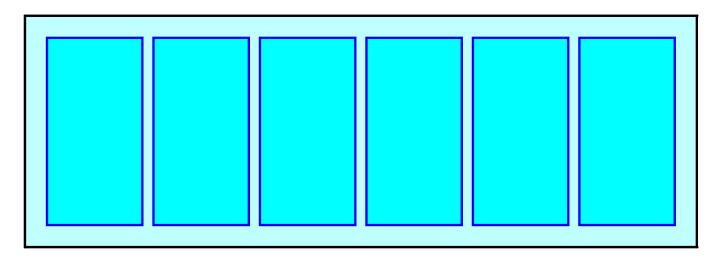
Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

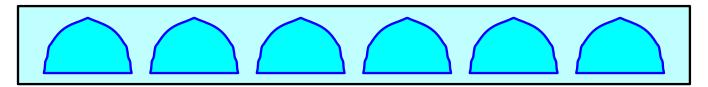
52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

- 1 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 8.50' Row Length +12.0" End Stone x 2 = 10.50' Base Length
- 6 Rows x 52.0" Wide + 6.0" Spacing x 5 + 12.0" Side Stone x 2 = 30.50' Base Width 6.0" Stone Base + 30.5" Chamber Height + 6.0" Stone Cover = 3.54' Field Height
- 6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 380.0 cf Chamber Storage
- 1,134.2 cf Field 380.0 cf Chambers = 754.2 cf Stone x 40.0% Voids = 301.7 cf Stone Storage

Chamber Storage + Stone Storage = 681.7 cf = 0.016 af Overall Storage Efficiency = 60.1% Overall System Size = 10.50' x 30.50' x 3.54'

6 Chambers 42.0 cy Field 27.9 cy Stone

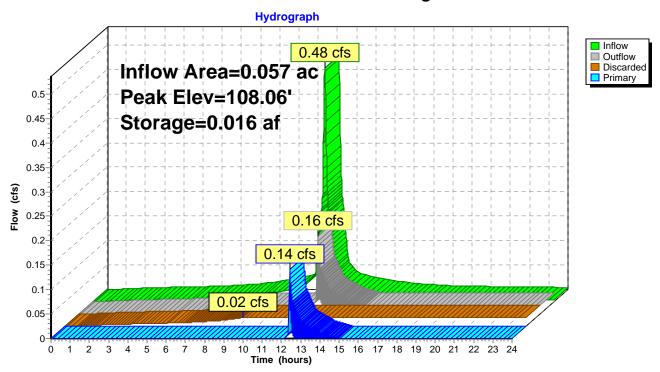




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Pond Lot 3: Roof Recharge



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Type III 24-hr 100-Year Rainfall=8.24" Printed 5/13/2024

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Summary for Pond Lot 4: Roof Recharge

Inflow Area =	0.057 ac,100.00% Impervious, Inflow D	epth > 7.99" for 100-Year event
Inflow =	0.48 cfs @ 12.07 hrs, Volume=	0.038 af
Outflow =	0.16 cfs @ 12.42 hrs, Volume=	0.030 af, Atten= 67%, Lag= 21.1 min
Discarded =	0.02 cfs @ 9.27 hrs, Volume=	0.027 af
Primary =	0.14 cfs @ 12.42 hrs, Volume=	0.003 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 108.06' @ 12.42 hrs Surf.Area= 0.007 ac Storage= 0.016 af

Plug-Flow detention time= 216.4 min calculated for 0.030 af (79% of inflow) Center-of-Mass det. time= 135.8 min (875.3 - 739.5)

Volume	Invert	Avail.Storage	Storage Description
#1A	103.00'	0.007 af	30.50'W x 10.50'L x 3.54'H Field A
			0.026 af Overall - 0.009 af Embedded = 0.017 af x 40.0% Voids
#2A	103.50'	0.009 af	Cultec R-330XLHD x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		0.016 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	103.00'	2.410 in/hr Exfiltration over Surface area
#2	Primary	108.00'	12.0" Horiz. Orifice/Grate C= 0.600
	•		I imited to weir flow at low heads

Discarded OutFlow Max=0.02 cfs @ 9.27 hrs HW=103.05' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=0.12 cfs @ 12.42 hrs HW=108.05' (Free Discharge) 2=Orifice/Grate (Weir Controls 0.12 cfs @ 0.74 fps)

2024-05-10_POST-DRAINAGE

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Pond Lot 4: Roof Recharge - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

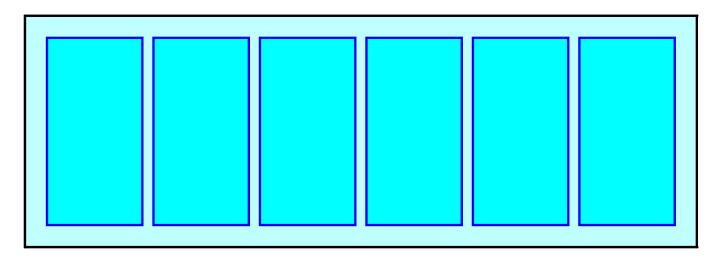
Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

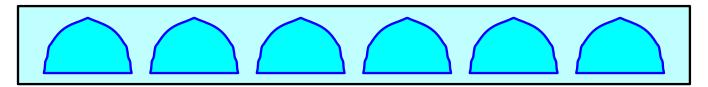
52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

- 1 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 8.50' Row Length +12.0" End Stone x 2 = 10.50' Base Length
- 6 Rows x 52.0" Wide + 6.0" Spacing x 5 + 12.0" Side Stone x 2 = 30.50' Base Width 6.0" Stone Base + 30.5" Chamber Height + 6.0" Stone Cover = 3.54' Field Height
- 6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 380.0 cf Chamber Storage
- 1,134.2 cf Field 380.0 cf Chambers = 754.2 cf Stone x 40.0% Voids = 301.7 cf Stone Storage

Chamber Storage + Stone Storage = 681.7 cf = 0.016 af Overall Storage Efficiency = 60.1% Overall System Size = 10.50' x 30.50' x 3.54'

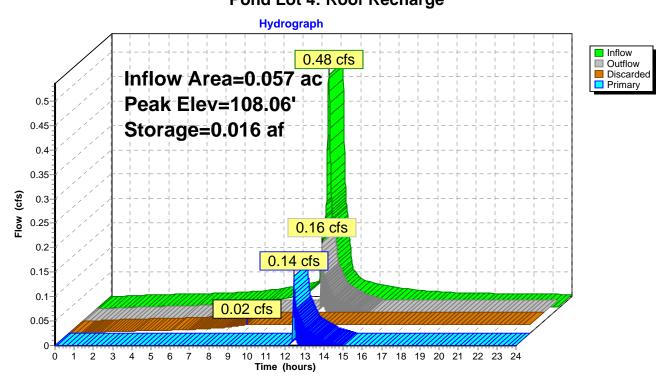
6 Chambers 42.0 cy Field 27.9 cy Stone





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Pond Lot 4: Roof Recharge



2024-05-10_POST-DRAINAGE

Type III 24-hr 100-Year Rainfall=8.24" Printed 5/13/2024

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Summary for Pond PR1: Recharge 1

Inflow Area =	1.077 ac, 34.35% Impervious, Inflow D	Depth > 5.96" for 100-Year event
Inflow =	6.18 cfs @ 12.15 hrs, Volume=	0.535 af
Outflow =	4.96 cfs @ 12.37 hrs, Volume=	0.393 af, Atten= 20%, Lag= 13.0 min
Discarded =	0.22 cfs @ 10.11 hrs, Volume=	0.277 af
Primary =	4.74 cfs @ 12.37 hrs, Volume=	0.116 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 109.57' @ 12.37 hrs Surf.Area= 0.089 ac Storage= 0.204 af

Plug-Flow detention time= 202.2 min calculated for 0.393 af (73% of inflow) Center-of-Mass det. time= 115.6 min (918.9 - 803.3)

Volume	Invert	Avail.Storage	Storage Description
#1A	103.00'	0.075 af	74.00'W x 52.50'L x 3.54'H Field A
			0.316 af Overall - 0.130 af Embedded = 0.186 af x 40.0% Voids
#2A	103.50'	0.130 af	Cultec R-330XLHD x 105 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 15 rows
		0.204 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	103.00'	2.410 in/hr Exfiltration over Surface area
#2	Primary	108.00'	12.0" Horiz. Orifice/Grate C= 0.600
			I imited to weir flow at low heads

Discarded OutFlow Max=0.22 cfs @ 10.11 hrs HW=103.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.22 cfs)

Primary OutFlow Max=4.74 cfs @ 12.37 hrs HW=109.57' (Free Discharge) 2=Orifice/Grate (Orifice Controls 4.74 cfs @ 6.04 fps)

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2024-05-10_POST-DRAINAGE

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Pond PR1: Recharge 1 - Chamber Wizard Field A

Chamber Model = Cultec R-330XLHD (Cultec Recharger® 330XLHD)

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 15 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

7 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 50.50' Row Length +12.0" End Stone x 2 = 52.50' Base Length

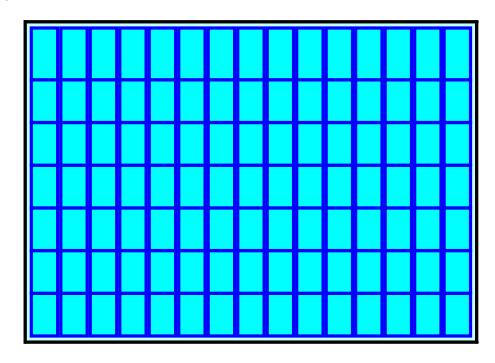
15 Rows x 52.0" Wide + 6.0" Spacing x 14 + 12.0" Side Stone x 2 = 74.00' Base Width 6.0" Stone Base + 30.5" Chamber Height + 6.0" Stone Cover = 3.54' Field Height

105 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 15 Rows = 5,644.1 cf Chamber Storage

13,759.4 cf Field - 5,644.1 cf Chambers = 8,115.2 cf Stone x 40.0% Voids = 3,246.1 cf Stone Storage

Chamber Storage + Stone Storage = 8,890.2 cf = 0.204 af Overall Storage Efficiency = 64.6% Overall System Size = 52.50' x 74.00' x 3.54'

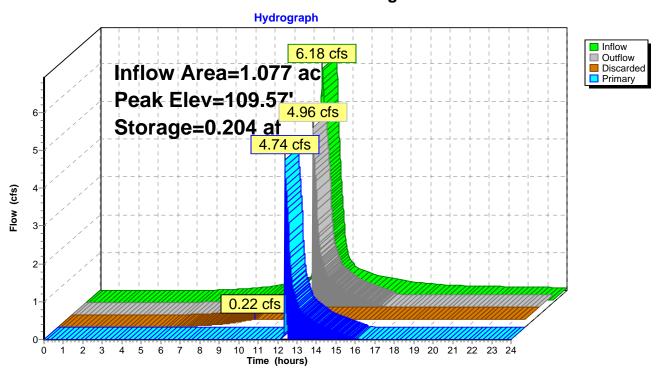
105 Chambers 509.6 cy Field 300.6 cy Stone





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Pond PR1: Recharge 1



Town of Reading Engineering Division

Memo

To: Andrew MacNichol , Community Development Director

From: Ryan A. Percival, P.E., Town Engineer;

CC: Community Planning and Development Commission;

Date: June 4, 2024

Re: Harold Avenue Extension

Materials reviewed:

- Definitive Subdivision Plan entitled; "Harold Avenue Extension", 0 Harold Avenue Reading, Massachusetts; prepared by Sullivan Engineering Group, LLC; dated November 4, 2023
- Drainage Analysis, Harold Avenue Extension; prepared by Sullivan Engineering Group, LLC; dated December 3, 2023

The Engineering Division has reviewed the proposed site application for the proposed project and offers the following comments:

- The subdivision plan appears to not meet proof. The plan does not conform to Section 7.1.2(a), "All angles in street lines shall be eased with curves having a center line radius of one hundred (100) feet minimum. Center lines of opposing streets shall be spaced a minimum of one hundred and fifty (150) feet apart. Reverse curves shall be separated with tangents having a minimum length of seventy-five feet".
- The stormwater design was based on the NOAA Atlas 14 rainfall frequencies. The post development runoff volumes for the 2-, 10-, 25- and 100-year storm have all been reduced. Post development peak discharge rates have been reduced except for the 100-year storm, which saw a slight increase.
- The Storm water design meets TSS removal at 90%
- The applicant shall provide phosphorus removal calculations.
- The size and type of the water and sewer service shall be shown on the plan.
- It is unclear what is happening with the drainage onsite. What is happening from DMH-1 down R1 to the round structure? Is this a catch basin?
- The garage floor elevation is lower than the surrounding area. A trench is proposed and should extend the entire width of the pavement. Was there consideration to raise the home to eliminate potential garage flooding?
- The Driveway width shall be labeled.
- Provide a detail of the retaining wall.
- All utilities shall be approved materials and installed in accordance with the Department of Public Works Standards.
- Engineering Division shall be notified 72 hours in advance to mark out Town utilities.
- All water, sewer, curb cut, street opening and Jackie's Law excavation permits shall be obtained at the Engineering Division prior to any excavations.
- All site work shall be inspected by the Engineering Division. The Applicant/Owner's contractor shall submit a
 construction schedule of proposed work. All inspections shall be scheduled 48 hours in advance.
- An approved site as-built shall be submitted to the Engineering Division within 60 days of certificate of occupancy. The as-built shall be submitted in mylar and electronic ACAD format

December 4, 2023

Town of Reading Planning Dept. 16 Lowell Street Reading, MA 01867

Re: 0 Harold Avenue Extension – Definitive Subdivision List of Waivers – Subdivision Rules & Regulations

Planning Department;

The following is a list of waivers from the Town of Reading Subdivision Rules and Regulations with supporting justification.

- 1. A waiver from Section 6.1.1.B.10 requiring existing topography of the tract and of all lands within 100 feet.
 - a. The applicant requests relief from this requirement due to limited area on a 4 acre parcel that is being disturbed to construct the house, driveway, utilities, and grading.
- 2. A waiver from Section 6.1.1.B.17 requiring a profile of existing and proposed grades along the centerline and ROW sidelines for all proposed streets and way.
 - a. The applicant requests a waiver from this requirement since no roadway is proposed.
- 3. A waiver from Section 6.1.1.C requiring a Way and Profile Plan
 - a. The applicant requests a waiver from this requirement since no roadway is proposed.
- 4. A waiver from Section 6.1.1.D(3) requiring a Traffic Study
 - a. The applicant requests relief from this requirement due to the modest scope of one additional single family home.
- 5. A waiver from Section 6.1.1.D(5) requiring test boring logs
 - a. The applicant requests a waiver from this requirement since no deep utility services are proposed
- 6. A waiver from Section 7.1.1.B requiring grades of streets
 - a. The applicant requests a waiver from this requirement since no roadway is proposed (only a driveway)
- 7. A waiver from Section 7.1.3 requiring street cross section
 - a. The applicant requests a waiver from this requirement since no roadway is proposed.
- 8. A waiver from Section 7.1.4(B) requiring the intersection of ways having a min. curbline radii of 30 feet.
 - a. The applicant requests a waiver from this requirement since the site has insufficient lot frontage to allow 30 foot radii. Since the applicant is only proposing one single family house to be accessed by a driveway a conventional radii rounding is not warranted.
- 9. A waiver from Section 7.1.5 requiring deadend streets to have a cul-de-sac.
 - a. The applicant requests a waiver from this requirement due to the limited scope of this project. In addition, the fire chief stated he would need a cul-de-sac in the case of 2 or more houses for this development. One single family house is being proposed.

- 10. A waiver from Section 7.1.7 requiring the installation of curbing
 - a. The applicant requests a waiver from this requirement since no roadway is being constructed
- 11. A waiver from Section 7.1.8 requiring the installation of monuments
 - a. The applicant requests a waiver from this requirement since this development will remain private.
- 12. A waiver from Section 7.1.9 requiring the installation of signs
 - a. A waiver from this requirement is requested since no signs are needed for the limited project.
- 13. A waiver from Section 7.1.11 requiring the installation of street lighting
 - a. A waiver from this requirement is requested due to the modest scope of work for this project and with one single family house that traditional lighting will suffice for safety.
- 14. A waiver from Section 7.2 requiring the installation of sidewalks
 - a. A waiver from this requirement is requested due to the limited scope of this project.
- 15. A waiver from Section 7.6 requiring the installation of street trees
 - a. A waiver is requested from this requirement since no roadway is proposed and the applicant has made an effort to save as many mature trees on site as possible
- 16. A waiver from Section 8.0 requiring the construction of a way
 - a. A waiver is requested from this requirement since no roadway is proposed.
- 17. A waiver from Section 6.1.1.D.4 requiring an Environmental Impact Study to be performed.
 - a. The applicant will be filing with the Reading Conservation Commission for review and approval with conditions for this project.

Sincerely,

Jack Sullivan, J

e-mail: jacksull53@comcast.net

December 3, 2023

Town of Reading Engineering Department

Re: Harold Avenue Extension – Reading, MA Drainage Analysis for CPDC submission

This drainage study was conducted at "Harold Avenue Extension" to evaluate the proposed Site development of the currently vacant lot. The existing site is predominately wooded with a dirt driveway. The proposed condition is for one single family house, paved driveway, and low impact development with attention to site preservation. The applicant is requesting waivers of the Subdivision Rules and Regulations to construct a 14 foot wide driveway in lieu of a conventional roadway/culdesac)

Soil testing was conducted on the site on May 4, 2023 and the soils were found to be suitable for drainage recharge (Loamy sand). The Existing Conditions Plan (Sheet 2) shows the testhole locations and the soil logs. An exfiltration rate of 1.02 in/hr is being used in the drainage analysis based on the Rawl's rate for a SANDY LOAM soil as a conservative approach to the stormwater design. The NRCS soil maps show this property being an "B" series soil. To mitigate the impact of the increase impervious surfaces with this site development a trench drain will be utilized for the driveway runoff with pretreatment of a deep sump manhole and rip-rap spreader prior to discharge to a raingarden. The rain garden is vertically sited 2 feet above the seasonal high groundwater table. The raingarden will have a rip-rap spillway to allow a controlled release of stormwater in larger storm events. The drainage system has been sized utilizing the 2, 10, 25, & 100 year storm numbers provided by NOAA.

IMPORTANT....this project will require filing with the Conservation Commission for review and approval. This drainage report will be supplemented at that time with the NOI stormwater report, drainage performance standards,

The HydroCAD report models the Predevelopment Condition vs. Postdevelopment Condition for the entire site area. The stormwater design reduces the peak rate of runoff for the 2, 10, 25, and 100 year storm event. The peak rate of stormwater runoff has been reduced for the 2 & 10 year storm event. The volume of stormwater runoff has been reduced in the 2, 10, 25, and 100 year storm. By reducing the stormwater volume in larger storm events will protect against flooding in accordance with the DEP stormwater requirements. The following is summary of the peak rate of runoff for various storm events:

	Predevelopment	Postdevelopment	Predevelopment	Postdevelopment
	Peak rate (cfs)	Peak rate (cfs)	Volume (AF)	Volume (AF)
Storm E	vent			
2 Year	0.43	0.05	0.047	0.007
10 Year	1.55	1.44	0.13	0.087
25 Year	2.81	3.27	0.223	0.181
100 Year	5.12	5.47	0.396	0.356

HydroCAD calculations with the accompanying subcatchment areas are attached to support these calculations. An operation and maintenance plan for the post development stormwater condition is attached to the end of this report.

Very Truly Yours,

John (Jack) D. Sullivan III, PE

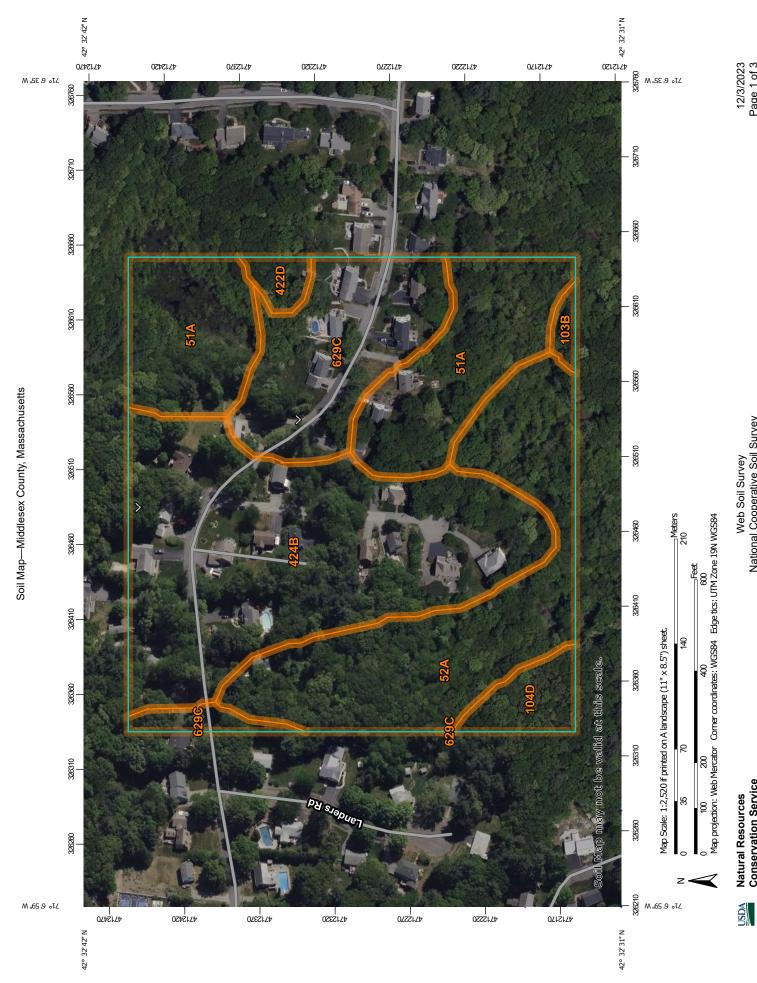
12323

PO Box 2004

Woburn, MA 01888 (781) 854-8644

SULLIVAN III

CIVIL

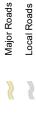


MAP LEGEND

Special Line Features Streams and Canals Very Stony Spot Stony Spot Spoil Area Wet Spot Other Rails Water Features **Fransportation** W 8 ŧ Soil Map Unit Polygons Area of Interest (AOI) Soil Map Unit Points Soil Map Unit Lines Special Point Features **Borrow Pit** Clay Spot Area of Interest (AOI) Blowout Soils

Closed Depression





Gravelly Spot

Gravel Pit



Marsh or swamp

Lava Flow

Landfill

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

Web Soil Survey URL:

distance and area. A projection that preserves area, such as the projection, which preserves direction and shape but distorts Albers equal-area conic projection, should be used if more This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Survey Area Data: Version 23, Sep 12, 2023

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: May 22, 2022—Jun

compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor

Severely Eroded Spot

Slide or Slip Sodic Spot

Sinkhole

Sandy Spot Saline Spot

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

MAP INFORMATION

contrasting soils that could have been shown at a more detailed misunderstanding of the detail of mapping and accuracy of soil Enlargement of maps beyond the scale of mapping can cause line placement. The maps do not show the small areas of

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator accurate calculations of distance or area are required.

Soil Survey Area: Middlesex County, Massachusetts

The orthophoto or other base map on which the soil lines were

shifting of map unit boundaries may be evident.

Map Unit Legend

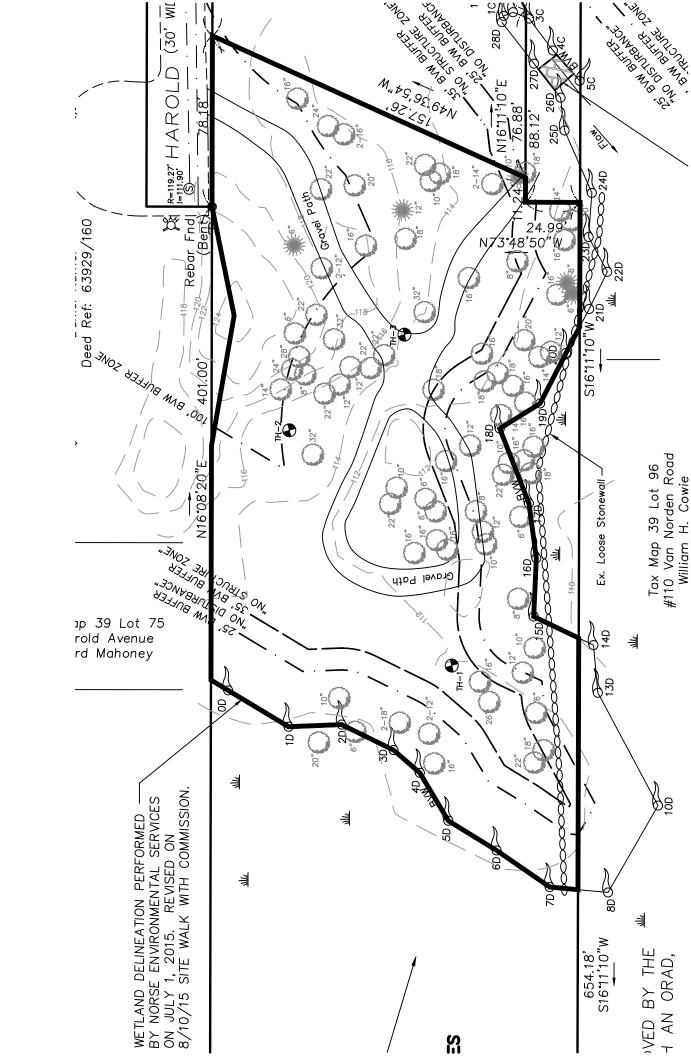
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
51A	Swansea muck, 0 to 1 percent slopes	4.9	20.8%
52A	Freetown muck, 0 to 1 percent slopes	5.3	22.5%
103B	Charlton-Hollis-Rock outcrop complex, 3 to 8 percent slopes	0.2	0.8%
104D	Hollis-Rock outcrop-Chariton complex, 15 to 25 percent slopes	0.7	3.1%
422D	Canton fine sandy loam, 15 to 35 percent slopes, extremely stony	0.3	1.4%
424B	Canton fine sandy loam, 3 to 8 percent slopes, extremely bouldery	8.5	36.3%
629C	Canton-Charlton-Urban land complex, 3 to 15 percent slopes	3.5	15.1%
Totals for Area of Interest		23.4	100.0%

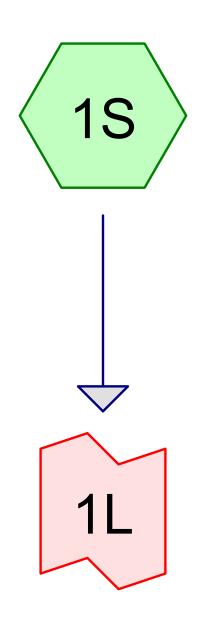
INSTRUCTIONS:

- In BMP Column, click on Blue Cell to Activate Drop Down Menu
 Select BMP from Drop Down Menu
 After BMP is selected, TSS Removal and other Columns are automatically completed.

_	В		BMP	1 Get Rain Garden	orksł	w no	culati	Cald			Prepa	
ocation:		,		den						Project:	Prepared By: Jps	Date:
_ocation: Harold Avenue Extension	O	TSS Removal	Rate ¹	0:30	0.00	0.00	0.00	0.00	Total T		JDS	Date: 12/3/2023
	Ω	Starting TSS	Load*	1.00	0.10	0.10	0.10	0.10	Total TSS Removal =	<u>.</u>		
	Ш	Amount	Removed (C*D)	0.90	0.00	0.00	0.00	0.00	%06		*Equals remaining load from previous BMP (E)	which enters the BMP
	ш	Remaining	Load (D-E)	0.10	0.10	0.10	0.10	0.10	Separate Form Needs to be Completed for Each Outlet or BMP Train		previous BMP (E)	

Non-automated TSS Calculation Sheet must be used if Proprietary BMP Proposed 1. From MassDEP Stormwater Handbook Vol. 1





Design Point 1









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Predevelopment

Type III 24-hr 2-Year Storm Rainfall=3.20"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S:

Runoff Area=47,217 sf Runoff Depth=0.52"

Flow Length=202' Tc=8.0 min CN=63 Runoff=0.43 cfs 0.047 af

Link 1L: Design Point 1

Inflow=0.43 cfs 0.047 af Primary=0.43 cfs 0.047 af

Total Runoff Area = 1.084 ac Runoff Volume = 0.047 af Average Runoff Depth = 0.52"

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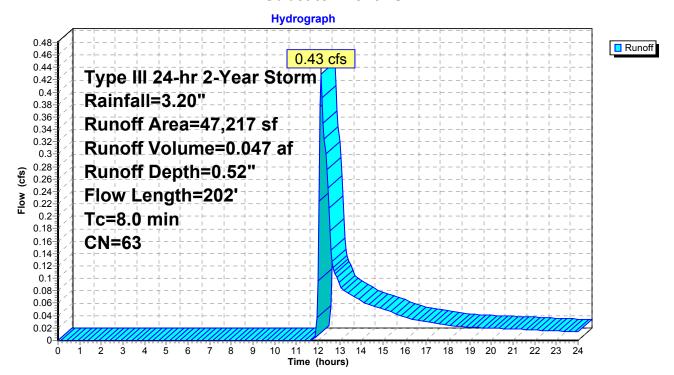
Subcatchment 1S:

Runoff = 0.43 cfs @ 12.15 hrs, Volume= 0.047 af, Depth= 0.52"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Storm Rainfall=3.20"

_	Α	rea (sf)	CN	Description		
		5,537		Dirt roads, I		
-	41,680 60 Woods, Fair, HSG B 47,217 63 Weighted Average				·	
	Tc (min)	Length (feet)	Slope (ft/ft	,	Capacity (cfs)	Description
_	5.4	50	0.1600	0.2		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.20"
	2.6	152	0.0390	1.0		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
-	8.0	202	Total			·

Subcatchment 1S:



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Link 1L: Design Point 1

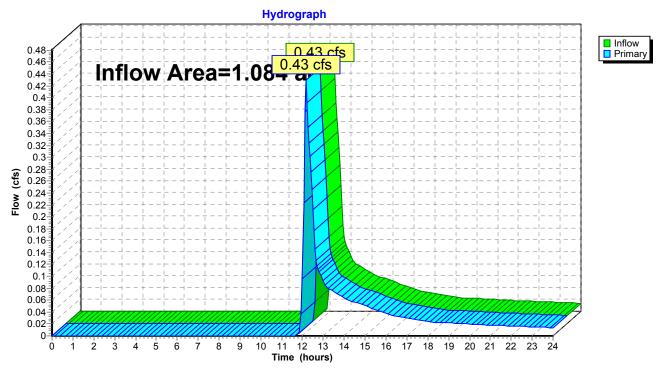
Inflow Area = 1.084 ac, Inflow Depth = 0.52" for 2-Year Storm event

Inflow = 0.43 cfs @ 12.15 hrs, Volume= 0.047 af

Primary = 0.43 cfs @ 12.15 hrs, Volume= 0.047 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Link 1L: Design Point 1



Predevelopment

Type III 24-hr 10-Year Storm Rainfall=4.90"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S:

Runoff Area=47,217 sf Runoff Depth=1.44"

Flow Length=202' Tc=8.0 min CN=63 Runoff=1.55 cfs 0.130 af

Link 1L: Design Point 1

Inflow=1.55 cfs 0.130 af Primary=1.55 cfs 0.130 af

Total Runoff Area = 1.084 ac Runoff Volume = 0.130 af Average Runoff Depth = 1.44"

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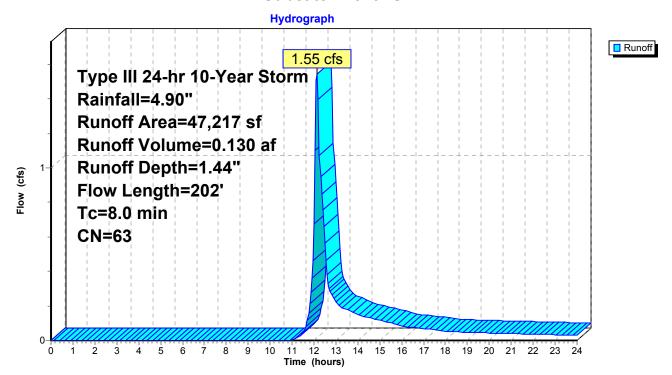
Subcatchment 1S:

Runoff = 1.55 cfs @ 12.13 hrs, Volume= 0.130 af, Depth= 1.44"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Storm Rainfall=4.90"

_	Α	rea (sf)	CN	Description		
5,537 82 Dirt roads, HSG B 41,680 60 Woods, Fair, HSG B						
47,217 63 Weighted Average					,	
	Tc (min)	Length (feet)	Slope (ft/ft)	•	Capacity (cfs)	Description
_	5.4	50	0.1600	0.2		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.20"
	2.6	152	0.0390	1.0		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
_	8.0	202	Total		_	

Subcatchment 1S:



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Link 1L: Design Point 1

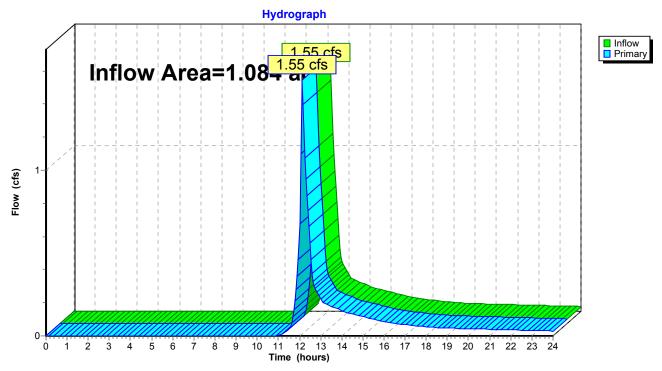
Inflow Area = 1.084 ac, Inflow Depth = 1.44" for 10-Year Storm event

Inflow = 1.55 cfs @ 12.13 hrs, Volume= 0.130 af

Primary = 1.55 cfs @ 12.13 hrs, Volume= 0.130 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Link 1L: Design Point 1



Predevelopment

Type III 24-hr 25-Year Storm Rainfall=6.41"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S:

Runoff Area=47,217 sf Runoff Depth=2.46"

Flow Length=202' Tc=8.0 min CN=63 Runoff=2.81 cfs 0.223 af

Link 1L: Design Point 1

Inflow=2.81 cfs 0.223 af Primary=2.81 cfs 0.223 af

Total Runoff Area = 1.084 ac Runoff Volume = 0.223 af Average Runoff Depth = 2.46"

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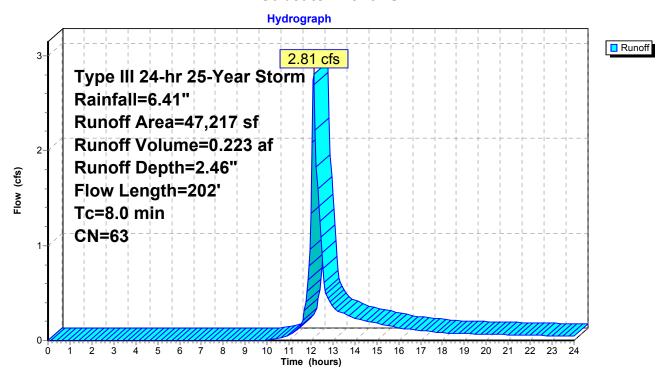
Subcatchment 1S:

Runoff = 2.81 cfs @ 12.12 hrs, Volume= 0.223 af, Depth= 2.46"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Storm Rainfall=6.41"

_	Α	rea (sf)	CN	Description		
5,537 82 Dirt roads, HSG B 41,680 60 Woods, Fair, HSG B						
47,217 63 Weighted Average					,	
	Tc (min)	Length (feet)	Slope (ft/ft)	•	Capacity (cfs)	Description
_	5.4	50	0.1600	0.2		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.20"
	2.6	152	0.0390	1.0		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
_	8.0	202	Total		_	

Subcatchment 1S:



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Link 1L: Design Point 1

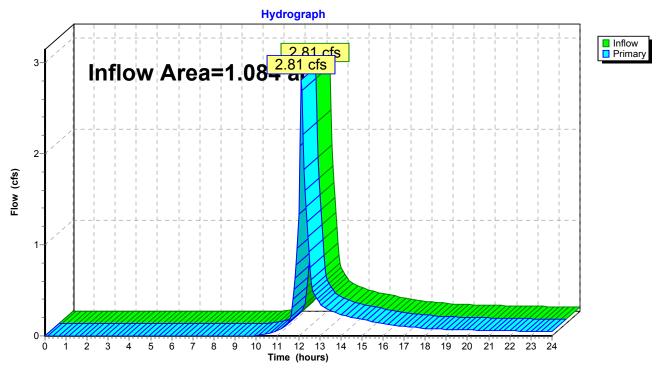
Inflow Area = 1.084 ac, Inflow Depth = 2.46" for 25-Year Storm event

Inflow = 2.81 cfs @ 12.12 hrs, Volume= 0.223 af

Primary = 2.81 cfs @ 12.12 hrs, Volume= 0.223 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Link 1L: Design Point 1



Predevelopment

Type III 24-hr 100-Year Storm Rainfall=8.90"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S:

Runoff Area=47,217 sf Runoff Depth=4.38"

Flow Length=202' Tc=8.0 min CN=63 Runoff=5.12 cfs 0.396 af

Link 1L: Design Point 1

Inflow=5.12 cfs 0.396 af Primary=5.12 cfs 0.396 af

Total Runoff Area = 1.084 ac Runoff Volume = 0.396 af Average Runoff Depth = 4.38"

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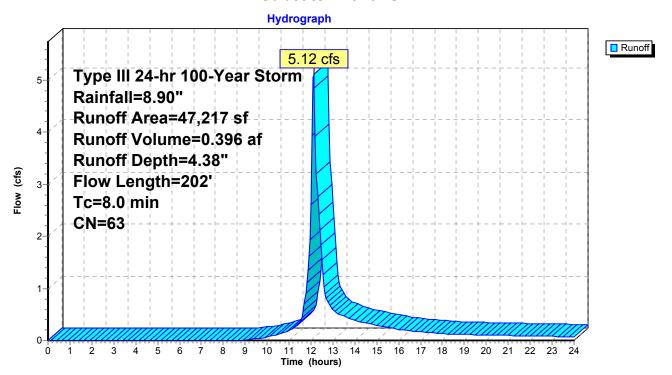
Subcatchment 1S:

Runoff = 5.12 cfs @ 12.12 hrs, Volume= 0.396 af, Depth= 4.38"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Storm Rainfall=8.90"

_	Α	rea (sf)	CN	Description		
5,537 82 Dirt roads, HSG B 41,680 60 Woods, Fair, HSG B						
47,217 63 Weighted Average					,	
	Tc (min)	Length (feet)	Slope (ft/ft)	•	Capacity (cfs)	Description
_	5.4	50	0.1600	0.2		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.20"
	2.6	152	0.0390	1.0		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
_	8.0	202	Total		_	

Subcatchment 1S:



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Link 1L: Design Point 1

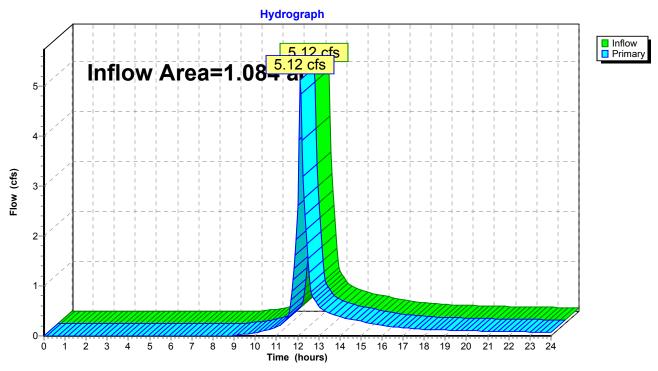
Inflow Area = 1.084 ac, Inflow Depth = 4.38" for 100-Year Storm event

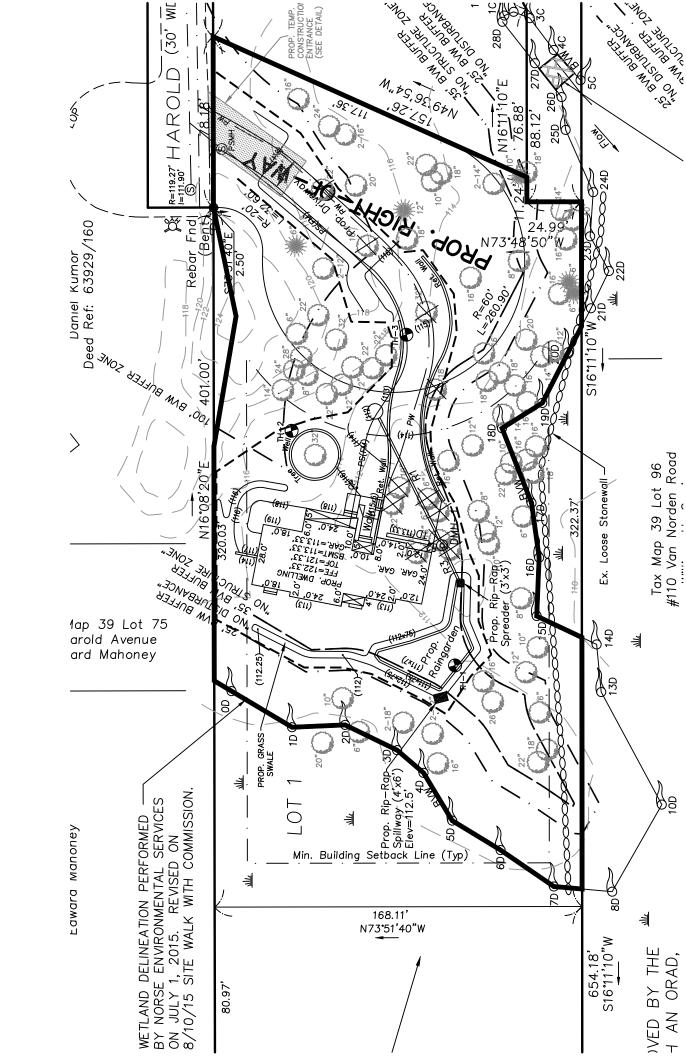
Inflow = 5.12 cfs @ 12.12 hrs, Volume= 0.396 af

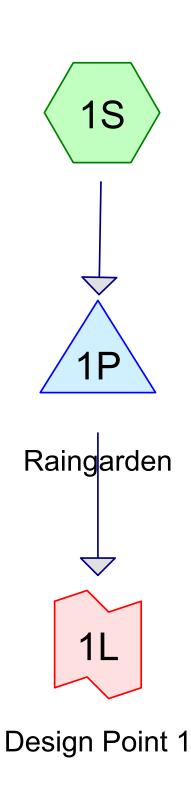
Primary = 5.12 cfs @ 12.12 hrs, Volume= 0.396 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Link 1L: Design Point 1















Drainage Diagram for postdevelopment
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postdevelopment

Type III 24-hr 2-Year Storm Rainfall=3.20"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S:

Runoff Area=47,217 sf Runoff Depth=0.60"

Flow Length=229' Tc=8.3 min CN=65 Runoff=0.54 cfs 0.054 af

Pond 1P: Raingarden

Peak Elev=112.52' Storage=967 cf Inflow=0.54 cfs 0.054 af

Discarded=0.03 cfs 0.031 af Primary=0.05 cfs 0.007 af Outflow=0.08 cfs 0.038 af

Link 1L: Design Point 1

Inflow=0.05 cfs 0.007 af Primary=0.05 cfs 0.007 af

Total Runoff Area = 1.084 ac Runoff Volume = 0.054 af Average Runoff Depth = 0.60"

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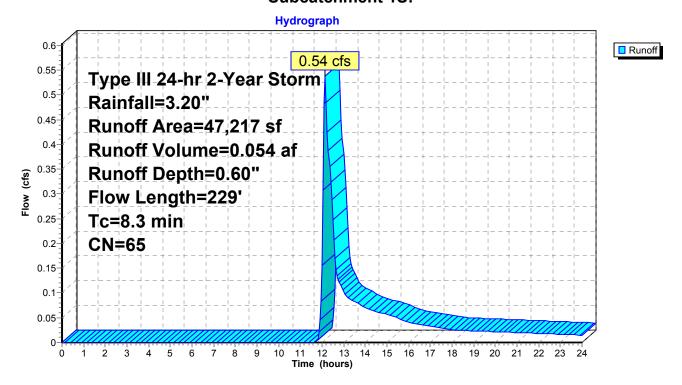
Subcatchment 1S:

Runoff = 0.54 cfs @ 12.15 hrs, Volume= 0.054 af, Depth= 0.60"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Storm Rainfall=3.20"

_	Α	rea (sf)	CN I	Description						
		2,458	98 I	House/Porch Roofs						
		170	98 v	walkway						
		3,685	98	oaved drive	way					
		217	98 ı	et wall						
		4,400	61	>75% Gras	s cover, Go	ood, HSG B				
_		36,287	60 \	Noods, Fai	r, HSG B					
		47,217	65 \	Neighted A	verage					
	Тс	Length	Slope		Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	5.4	50	0.1600	0.2		Sheet Flow,				
						Woods: Light underbrush n= 0.400 P2= 3.20"				
	2.9	179	0.0220	1.0		Shallow Concentrated Flow,				
						Short Grass Pasture Kv= 7.0 fps				
	8.3	229	Total			•				

Subcatchment 1S:



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Pond 1P: Raingarden

Inflow Area = 1.084 ac, Inflow Depth = 0.60" for 2-Year Storm event

Inflow = 0.54 cfs @ 12.15 hrs, Volume= 0.054 af

Outflow = 0.08 cfs @ 13.69 hrs, Volume= 0.038 af, Atten= 85%, Lag= 92.5 min

Discarded = 0.05 cfs @ 13.69 hrs, Volume= 0.007 af

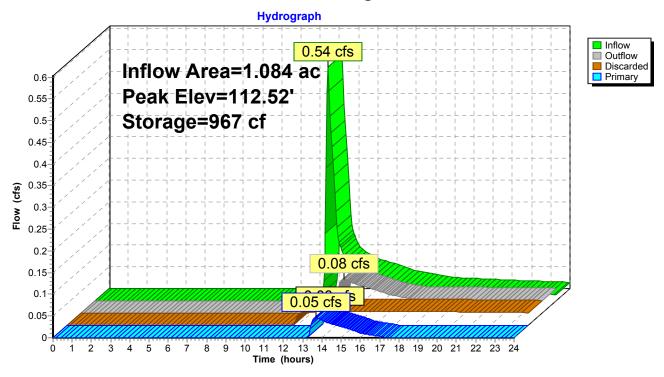
Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 112.52' @ 13.69 hrs Surf.Area= 1,383 sf Storage= 967 cf Plug-Flow detention time= 252.5 min calculated for 0.038 af (70% of inflow) Center-of-Mass det. time= 144.3 min (1,040.5 - 896.2)

#_	Invert	Avail.S	torage Stor	age Descri	ption			
1	111.70'	1,	241 cf Cus	tom Stage	Data (Prism	atic)Listed below		
Elevation (feet)		Surf.Area (sq-ft)		Store feet)	Cum.Store (cubic-feet)			
111.70		718		0	0			
111.75		868		40	40			
112.75		1,535	1	,202	1,241			
#	<u>_</u>		Outlet Devic					
1	Discarded	0.00'	-			ire Surface area		
2	Primary	112.50'	6.0' long x 4.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.5 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.38 2.54 2.69 2.68 2.67 2.67 2.65 2.66 2.66 2.68 2.72 2.73 2.76 2.79 2.88 3.07 3.32					

Discarded OutFlow Max=0.03 cfs @ 13.69 hrs HW=112.52' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.03 cfs)

Primary OutFlow Max=0.05 cfs @ 13.69 hrs HW=112.52' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 0.05 cfs @ 0.3 fps)

Pond 1P: Raingarden



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Link 1L: Design Point 1

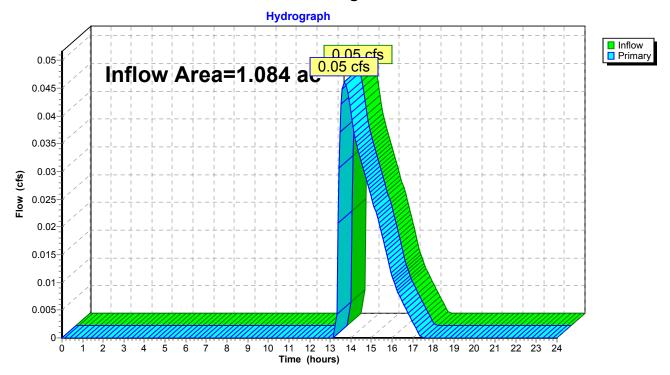
Inflow Area = 1.084 ac, Inflow Depth = 0.08" for 2-Year Storm event

Inflow = 0.05 cfs @ 13.69 hrs, Volume= 0.007 af

Primary = 0.05 cfs @ 13.69 hrs, Volume= 0.007 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Link 1L: Design Point 1



postdevelopment

Type III 24-hr 10-Year Storm Rainfall=4.90"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S:

Runoff Area=47,217 sf Runoff Depth=1.58"

Flow Length=229' Tc=8.3 min CN=65 Runoff=1.72 cfs 0.143 af

Pond 1P: Raingarden

Peak Elev=112.72' Storage=1,201 cf Inflow=1.72 cfs 0.143 af

Discarded=0.04 cfs 0.034 af Primary=1.44 cfs 0.087 af Outflow=1.47 cfs 0.122 af

Link 1L: Design Point 1

Inflow=1.44 cfs 0.087 af Primary=1.44 cfs 0.087 af

Total Runoff Area = 1.084 ac Runoff Volume = 0.143 af Average Runoff Depth = 1.58"

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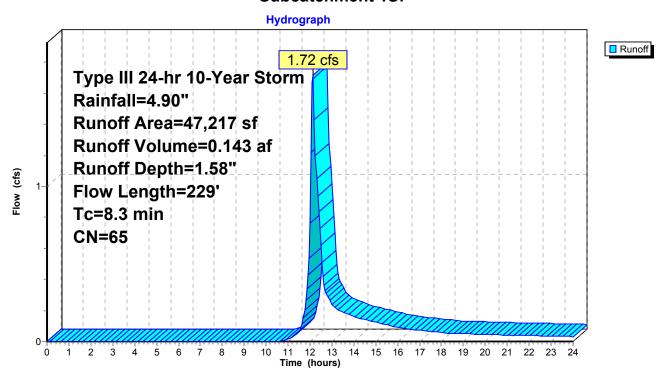
Subcatchment 1S:

Runoff = 1.72 cfs @ 12.13 hrs, Volume= 0.143 af, Depth= 1.58"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Storm Rainfall=4.90"

A	rea (sf)	CN	Description								
	2,458	98	98 House/Porch Roofs								
	170	98	walkway								
	3,685	98	paved driveway								
	217	98	ret wall								
4,400 61 >75% Grass cover, Good, HSG B											
	36,287	60	Woods, Fai	r, HSG B							
	47,217 65 Weighted Average										
Tc	Length	Slope		Capacity	Description						
(min)	(feet)	(ft/ft)) (ft/sec)	(cfs)							
5.4	50 0.1600 0.2				Sheet Flow,						
					Woods: Light underbrush n= 0.400 P2= 3.20"						
2.9	179	0.0220	1.0		Shallow Concentrated Flow,						
					Short Grass Pasture Kv= 7.0 fps						
8.3	229	Total									

Subcatchment 1S:



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Pond 1P: Raingarden

Inflow Area = 1.084 ac, Inflow Depth = 1.58" for 10-Year Storm event
Inflow = 1.72 cfs @ 12.13 hrs, Volume= 0.143 af
Outflow = 1.47 cfs @ 12.22 hrs, Volume= 0.122 af, Atten= 14%, Lag= 5.3 min
Discarded = 0.04 cfs @ 12.22 hrs, Volume= 0.034 af
Primary = 1.44 cfs @ 12.22 hrs, Volume= 0.087 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 112.72' @ 12.22 hrs Surf.Area= 1,513 sf Storage= 1,201 cf Plug-Flow detention time= 96.9 min calculated for 0.122 af (85% of inflow) Center-of-Mass det. time= 30.4 min (893.7 - 863.2)

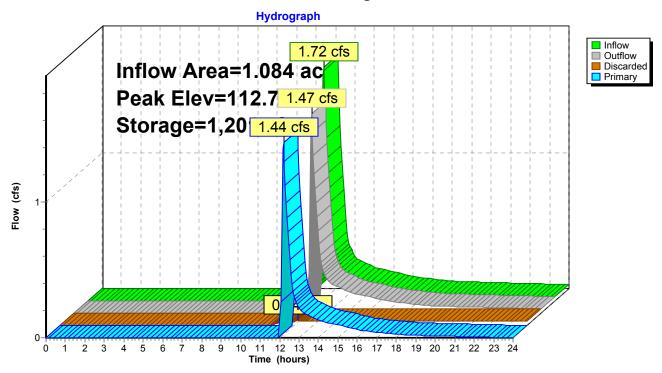
#_	Invert	Avail.S	torage Sto	orage Descri	ption	
1	111.70'	1,	241 cf Cu	stom Stage	Data (Prism	atic)Listed below
Elevation (feet)		Surf.Area (sq-ft)		.Store c-feet)	Cum.Store (cubic-feet)	
111.70		718		0	0	
111.75		868		40	40	
112.75		1,535		1,202	1,241	
#	Routing	Invert	Outlet Devi			in Ourface and
1	Discarded	0.00'		•		re Surface area
2	Primary	112.50'	Head (feet) 3.00 3.50 Coef. (Eng) 0.20 0.40 4.00 4.50 (lish) 2.38 2	0.60 0.80 1 5.00 5.50	sted Rectangular Weir .00 1.20 1.40 1.60 1.80 2.00 2.50 8 2.67 2.67 2.65 2.66 2.66 2.68 32

Discarded OutFlow Max=0.04 cfs @ 12.22 hrs HW=112.71' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.04 cfs)

Primary OutFlow Max=1.35 cfs @ 12.22 hrs HW=112.71' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 1.35 cfs @ 1.1 fps)

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Pond 1P: Raingarden



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Link 1L: Design Point 1

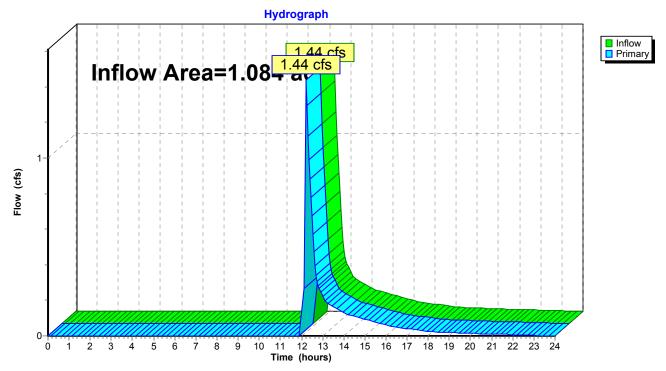
Inflow Area = 1.084 ac, Inflow Depth = 0.97" for 10-Year Storm event

Inflow = 1.44 cfs @ 12.22 hrs, Volume= 0.087 af

Primary = 1.44 cfs @ 12.22 hrs, Volume= 0.087 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Link 1L: Design Point 1



postdevelopment

Type III 24-hr 25-Year Storm Rainfall=6.41"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S:

Runoff Area=47,217 sf Runoff Depth=2.65"

Flow Length=229' Tc=8.3 min CN=65 Runoff=3.02 cfs 0.239 af

Pond 1P: Raingarden

Peak Elev=112.86' Storage=1,241 cf Inflow=3.02 cfs 0.239 af

Discarded=0.04 cfs 0.036 af Primary=3.27 cfs 0.181 af Outflow=3.31 cfs 0.217 af

Link 1L: Design Point 1

Inflow=3.27 cfs 0.181 af Primary=3.27 cfs 0.181 af

Total Runoff Area = 1.084 ac Runoff Volume = 0.239 af Average Runoff Depth = 2.65"

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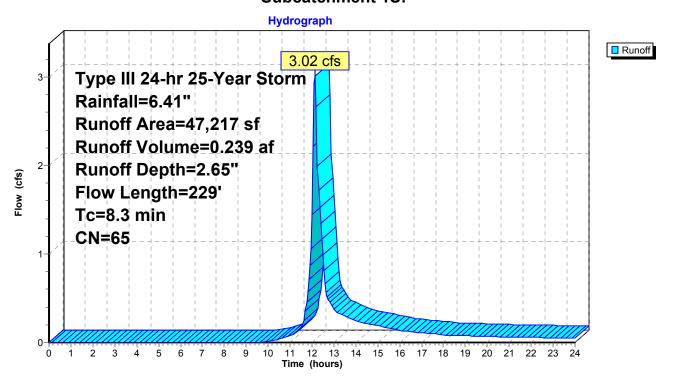
Subcatchment 1S:

Runoff = 3.02 cfs @ 12.12 hrs, Volume= 0.239 af, Depth= 2.65"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Storm Rainfall=6.41"

	Δ	rea (sf)	CN	Description								
		2,458										
		,										
		170		walkway								
		3,685	98	8 paved driveway								
	217 98 ret wall											
4,400 61 >75% Grass cover, Good, HSG B												
		36,287		Woods, Fai		,						
	47,217 65 Weighted Average											
	Tc	Length	Slope	e Velocity	Capacity	Description						
	(min)	(feet)	(ft/ft)		(cfs)	•						
5.4 50 0.1600 0.2						Sheet Flow,						
Woods: Light underbrush n= 0.400 P2=												
2.9 179 0.0220 1.0						Shallow Concentrated Flow,						
	2.5	173	0.0220	1.0		•						
_						Short Grass Pasture Kv= 7.0 fps						
	8.3	229	Total									

Subcatchment 1S:



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Pond 1P: Raingarden

Inflow Area = 1.084 ac, Inflow Depth = 2.65" for 25-Year Storm event
Inflow = 3.02 cfs @ 12.12 hrs, Volume= 0.239 af
Outflow = 3.31 cfs @ 12.11 hrs, Volume= 0.217 af, Atten= 0%, Lag= 0.0 min
Discarded = 0.04 cfs @ 12.10 hrs, Volume= 0.036 af
Primary = 3.27 cfs @ 12.11 hrs, Volume= 0.181 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 112.86' @ 12.11 hrs Surf.Area= 1,535 sf Storage= 1,241 cf Plug-Flow detention time= 63.1 min calculated for 0.217 af (91% of inflow) Center-of-Mass det. time= 18.2 min (865.9 - 847.7)

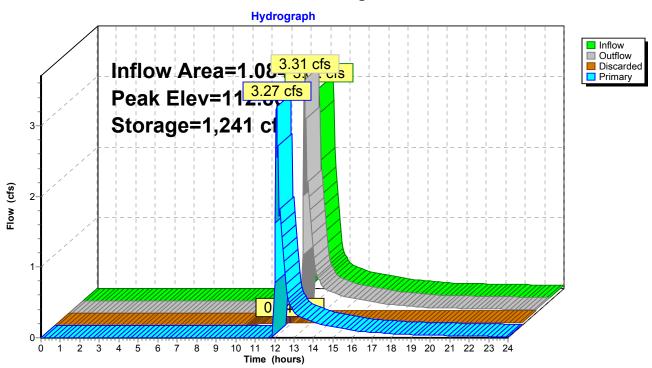
#	Invert	Avail.S	Avail.Storage		escription	
1	111.70'	1,241 cf		Custom St	tage Data (Prism	atic)Listed below
Elevation (feet) 111.70 111.75 112.75		Surf.Area (sq-ft) 718 868 1,535	(0	Inc.Store cubic-feet) 0 40 1,202	Cum.Store (cubic-feet) 0 40 1,241	
#	# Routing Invert		Outlet I	Devices		
1	Discarded	0.00'	0.00' 0.001416 fpm Exfiltration over entire			ire Surface area
2 Primary 112.50' 6.0' long x 4.0' breadth Broad-Crested Recta Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.38 2.54 2.69 2.68 2.67 2.6 2.72 2.73 2.76 2.79 2.88 3.07 3.32						1.00 1.20 1.40 1.60 1.80 2.00 2.50 68 2.67 2.67 2.65 2.66 2.66 2.68

Discarded OutFlow Max=0.04 cfs @ 12.10 hrs HW=112.86' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.04 cfs)

Primary OutFlow Max=3.08 cfs @ 12.11 hrs HW=112.85' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 3.08 cfs @ 1.5 fps)

12/3/2023

Pond 1P: Raingarden



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Link 1L: Design Point 1

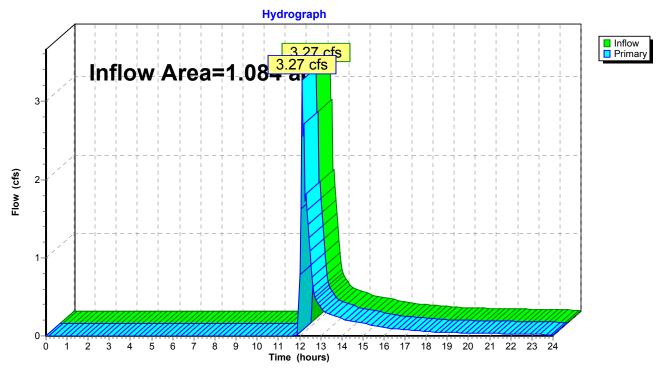
Inflow Area = 1.084 ac, Inflow Depth = 2.01" for 25-Year Storm event

Inflow = 3.27 cfs @ 12.11 hrs, Volume= 0.181 af

Primary = 3.27 cfs @ 12.11 hrs, Volume= 0.181 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Link 1L: Design Point 1



postdevelopment

Type III 24-hr 100-Year Storm Rainfall=8.90"

Prepared by Sullivan Engineering Group, LLC

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12/3/2023

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S:

Runoff Area=47,217 sf Runoff Depth=4.63"

Flow Length=229' Tc=8.3 min CN=65 Runoff=5.36 cfs 0.418 af

Pond 1P: Raingarden

Peak Elev=113.00' Storage=1,241 cf Inflow=5.36 cfs 0.418 af

Discarded=0.04 cfs 0.040 af Primary=5.47 cfs 0.356 af Outflow=5.51 cfs 0.396 af

Link 1L: Design Point 1

Inflow=5.47 cfs 0.356 af

Primary=5.47 cfs 0.356 af

Total Runoff Area = 1.084 ac Runoff Volume = 0.418 af Average Runoff Depth = 4.63"

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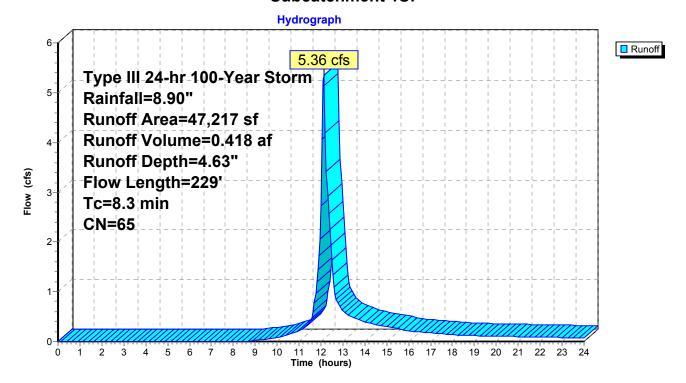
Subcatchment 1S:

Runoff = 5.36 cfs @ 12.12 hrs, Volume= 0.418 af, Depth= 4.63"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Storm Rainfall=8.90"

	Δ	rea (sf)	CN	Description								
		2,458										
		,										
		170		walkway								
		3,685	98	8 paved driveway								
	217 98 ret wall											
4,400 61 >75% Grass cover, Good, HSG B												
		36,287		Woods, Fai		,						
	47,217 65 Weighted Average											
	Tc	Length	Slope	e Velocity	Capacity	Description						
	(min)	(feet)	(ft/ft)		(cfs)	•						
5.4 50 0.1600 0.2						Sheet Flow,						
Woods: Light underbrush n= 0.400 P2=												
2.9 179 0.0220 1.0						Shallow Concentrated Flow,						
	2.5	173	0.0220	1.0		•						
_						Short Grass Pasture Kv= 7.0 fps						
	8.3	229	Total									

Subcatchment 1S:



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Pond 1P: Raingarden

Inflow Area = 1.084 ac, Inflow Depth = 4.63" for 100-Year Storm event
Inflow = 5.36 cfs @ 12.12 hrs, Volume= 0.418 af
Outflow = 5.51 cfs @ 12.11 hrs, Volume= 0.396 af, Atten= 0%, Lag= 0.0 min
Discarded = 0.04 cfs @ 11.95 hrs, Volume= 0.040 af
Primary = 5.47 cfs @ 12.11 hrs, Volume= 0.356 af

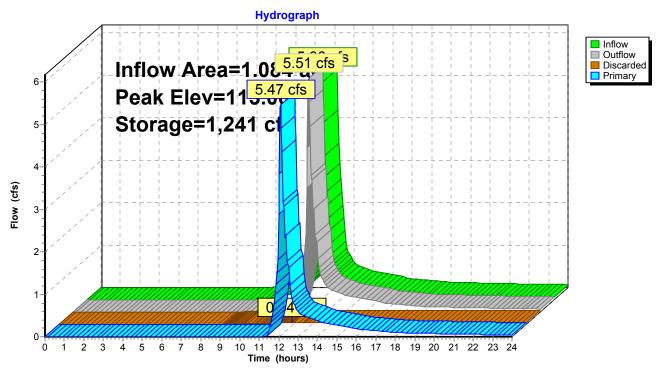
Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 113.00' @ 12.11 hrs Surf.Area= 1,535 sf Storage= 1,241 cf Plug-Flow detention time= 40.7 min calculated for 0.395 af (95% of inflow) Center-of-Mass det. time= 12.6 min (844.1 - 831.6)

#	Invert	Avail.Storage		torage Des	scription			
1	111.70'	1,241 cf		ustom Sta	age Data (Prisma	atic)Listed below		
Elevation (feet)		Surf.Area (sq-ft)		c.Store ic-feet)	Cum.Store (cubic-feet)			
111.70		718		0	0			
111.75		868		40	40			
11	12.75	1,535		1,202	1,241			
#	Routing Invert		Outlet De	vices				
1	Discarded	0.00'	0.00' 0.001416 fpm Exfiltration over entire Surface area					
2 Primary 112.50' 6.0' long x 4.0' breadth Broad-Crested Rectangula Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.38 2.54 2.69 2.68 2.67 2.67 2.69 2.72 2.73 2.76 2.79 2.88 3.07 3.32						.60 1.80		

Discarded OutFlow Max=0.04 cfs @ 11.95 hrs HW=112.75' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.04 cfs)

Primary OutFlow Max=5.27 cfs @ 12.11 hrs HW=112.98' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 5.27 cfs @ 1.8 fps)

Pond 1P: Raingarden



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Link 1L: Design Point 1

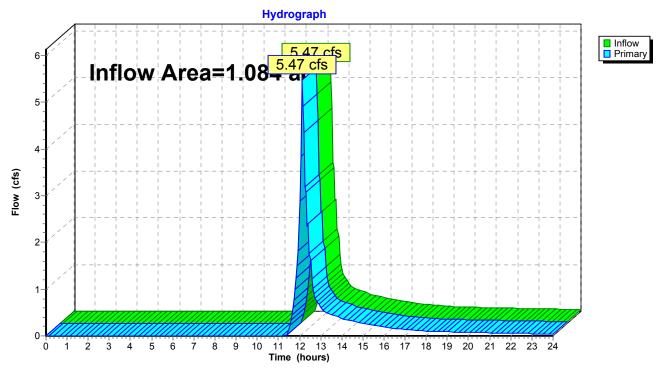
Inflow Area = 1.084 ac, Inflow Depth = 3.94" for 100-Year Storm event

Inflow = 5.47 cfs @ 12.11 hrs, Volume= 0.356 af

Primary = 5.47 cfs @ 12.11 hrs, Volume= 0.356 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Link 1L: Design Point 1

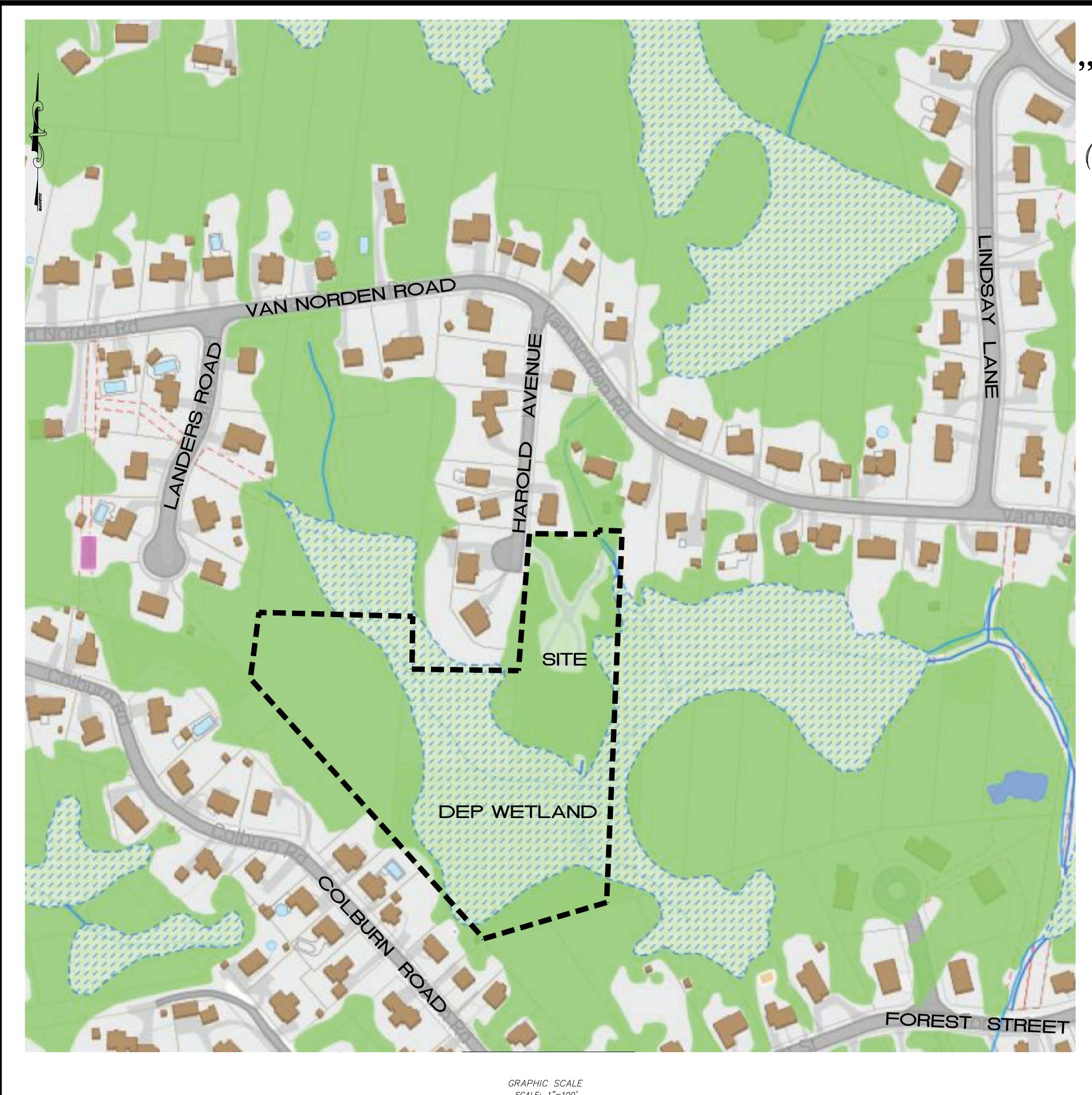


Post-Construction Stormwater Maintenance Plan

Beginning with the construction of the drainage system, and continuing in perpetuity thereafter, the owner(s) of the site shall maintain in accordance with the following schedule:

- a. Driveway sweeping and snow plowing Pavement and walkways shall be swept in the early spring immediately after snow melt and at least twice other times annually. Snow shall be plowed onto the snow stockpile area shown on the design plans to encourage infiltration during subsequent thawing periods. Sediments shall be removed from snow storage areas in the early spring.
- b. Paving Paving shall be maintained in good condition to channel surface runoff into the stormwater management facilities.
- c. Roof drain inlets, downspouts, and roof drain pipes All components of the roof drain collection system shall be inspected at least 3 times per year. Sediments and debris shall be removed and disposed of in accordance with all applicable federal, state, and local laws. Any components that become damaged shall be repaired or replaced immediately upon discovery to assure proper conveyance of stormwater runoff into the subsurface infiltration system.
- d. Rain Gardens The level of water in the Rain Gardens shall be monitored during and after heavy rain storms at least 3 times per year during the first year of operation and at least twice annually thereafter for evidence of clogging or other problems. The emergency overflow devices (spillway) shall be monitored to insure each is functioning properly and free of any obstructions.
- e. Vegetation shall be maintained in healthy condition to prevent erosion and sedimentation in the drainage system and off-site wetland resource areas. The vegetation in the 'Rain Gardens' shall be maintained as native plants and/or shrubs, and shall not be converted to a mowed lawn or other use. Additionally, the post and rail fencing partial surrounding the rain garden shall be inspected 3 times per year to insure the fencing is intact.
- f. Rip-Rap Pretreatment Area & Emergency Overflow spillway shall be inspected 3 times per year to insure any debris, trash, accumulated sediment, or leaves is removed and properly disposed of to insure functionality of these areas.

The Annual Stormwater Report (and repair information if performed) shall be submitted to the Town of Reading Engineering Department by January 15th of each calendar year.



DEFINITIVE SUBDIVISION PLAN 'HAROLD AVENUE EXTENSION'

O HAROLD AVENUE

(PORTION OF TAX MAP 39 LOT 230)

LOCATED IN

READING, MASSACHUSETTS

(MIDDLESEX COUNTY)

DATE: NOVEMBER 4, 2023

OWNER/APPLICANT:

ZERO HAROLD AVENUE, LLC

BRICKLEY/SEAR, P.A.

75 FEDERAL STREET, SUITE 1320 BOSTON, MA 02110 (617) 542-0896

ENGINEER:

SULLIVAN ENGINEERING GROUP, LLC

P.O. BOX 2004 WOBURN, MA 01888 (781) 854-8644

ATTORNEY:

JOHN E. SUTHERLAND

BRICKLEY/SEARS, P.A.

75 FEDERAL STREET, SUITE 1320 BOSTON, MA 02110 (617) 542-0896

LIST OF SUBDIVISION WAIVERS:

SECTION 6.1.1.B.10 — EXISTING TOPOGRAPHY OF THE TRACT AND OF ALL LANDS WITHIN 100 FEET SECTION 6.1.1.B.17- A PROFILE OF EXISTING AND PROPOSED GRADES ALONG THE CENTERLINE AND R.O.W. SIDELINES FOR ALL PROPOSED STREETS AND WAYS.

SECTION 6.1.1.C WAY AND PROFILE PLAN

SECTION 6.1.1.D(3) - TRAFFIC STUDY

SECTION 6.1.1.D(5) - TEST BORING LOGS

SECTION 7.1.1.B - GRADES OF STREETS

SECTION 7.1.3 - STREET CROSS SECTION

SECTION 7.1.4(B) - INTERSECTION OF WAYS - MIN. CURBLINE RADII OF 30 FEET

SECTION 7.1.5 - DEAD END STREETS/CUL-DE-SACS

SECTION 7.1.7 - CURBING

SECTION 7.1.8 - MONUMENTS

SECTION 7.1.9 - SIGNS SECTION 7.1.11 - STREET LIGHTING

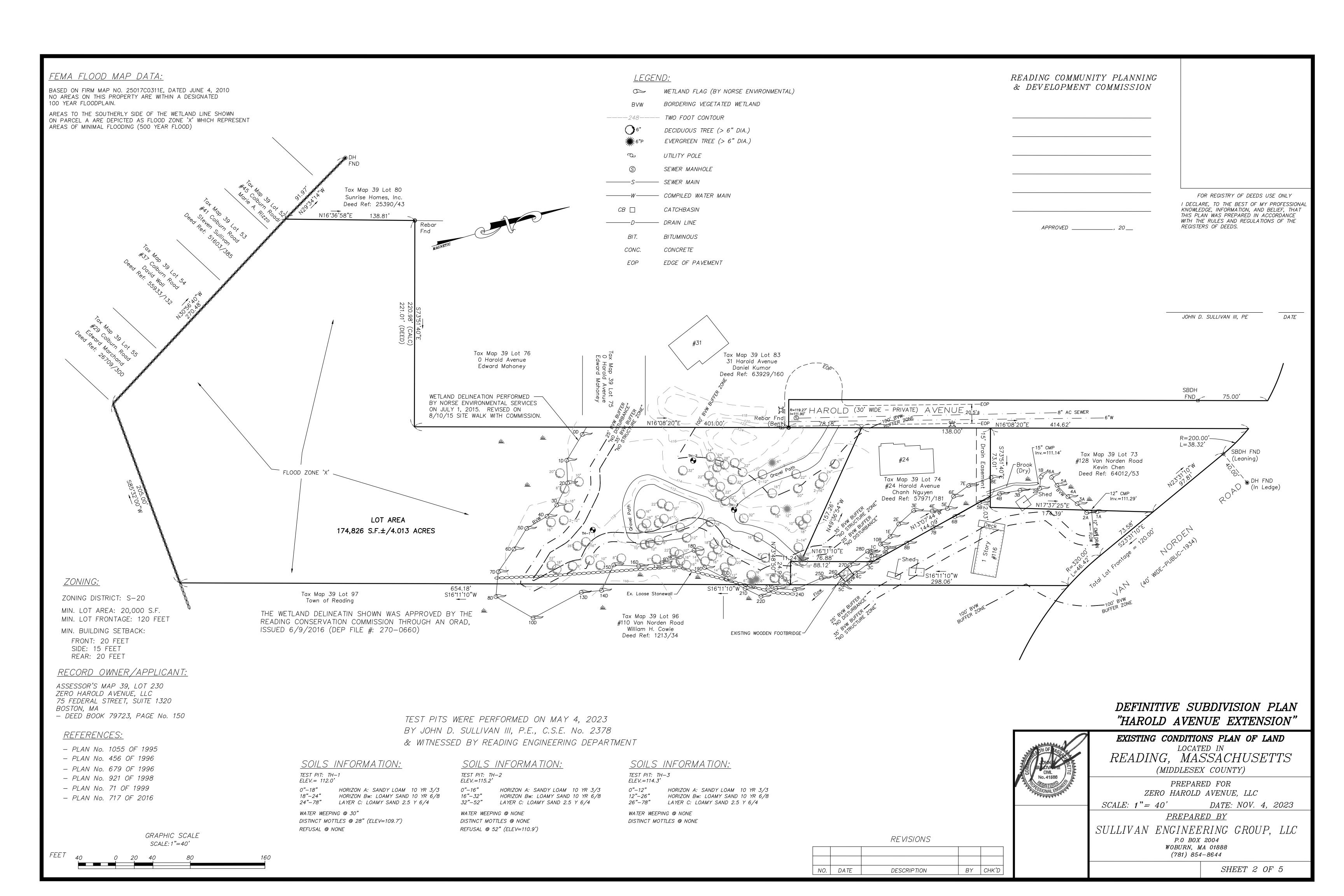
SECTION 7.2 - SIDEWALK

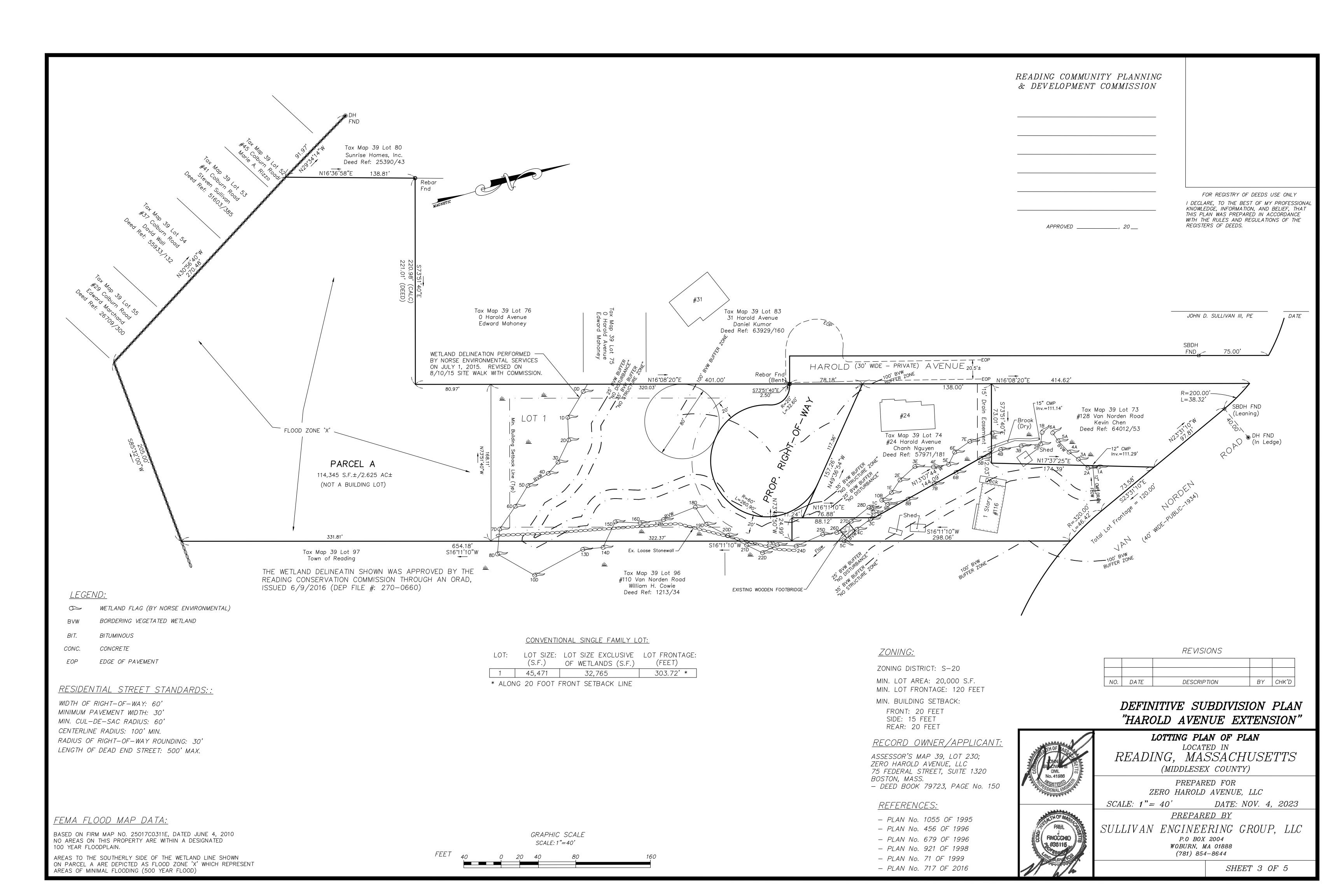
SECTION 7.6 - STREET TREES

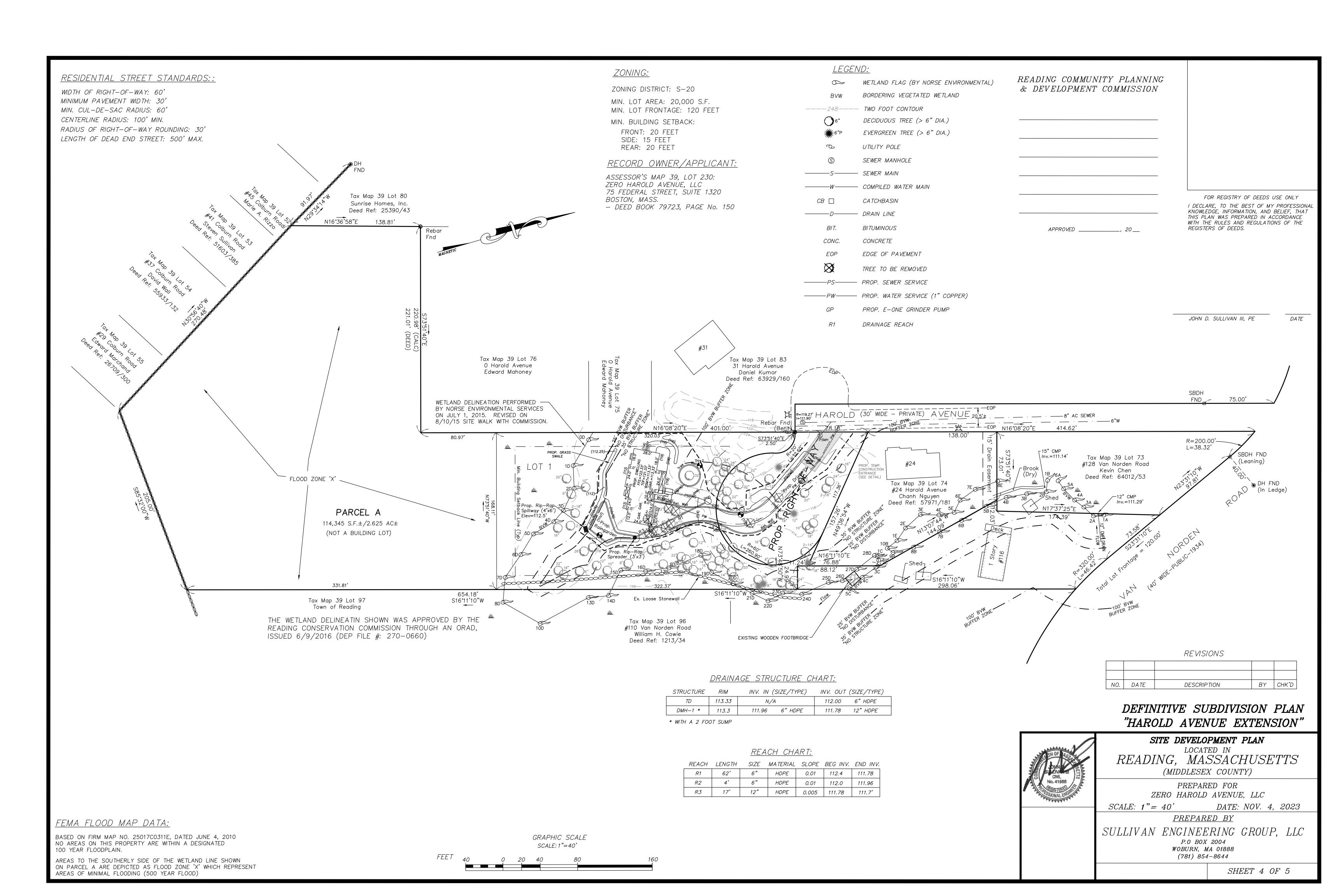
SECTION 8.0 - CONSTRUCTION OF WAYS

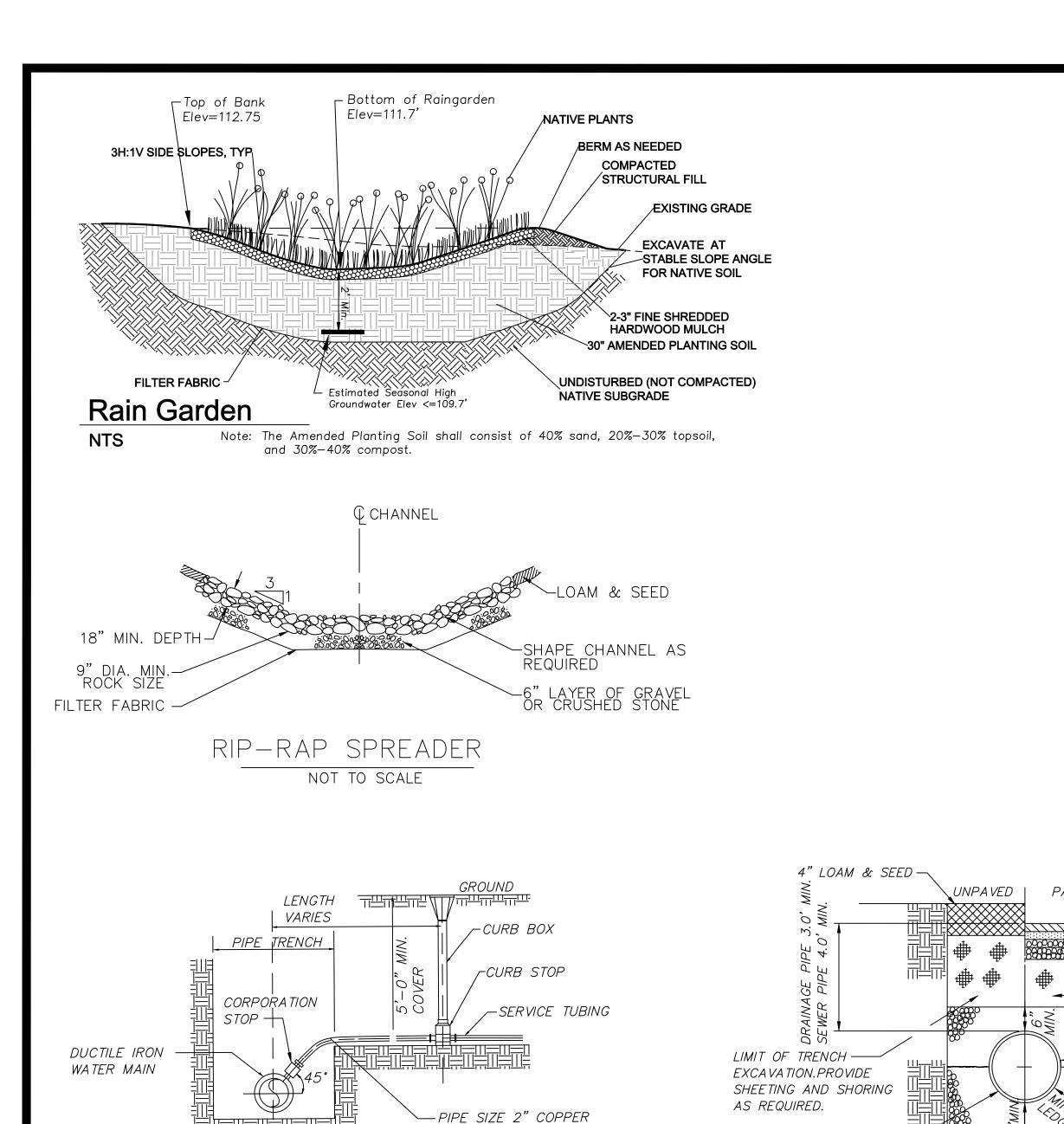
SHEET INDEX:

- COVER SHEET & LOCUS MAP
- EXISTING CONDITIONS
- LOTTING PLAN OF LAND
- SITE DEVELOPMENT PLAN
- 5 CONSTRUCTION DETAILS









SOLID SLEEVE COUPLING

SEE PAVEMENT DETAILS AND SPECS.

-GRAVEL BORROW COMPACTED IN 12"

MDPW SPEC. M1.03.0 TYPE A

MASS. D.P.W. M1.04.0 TYPE B

USING A HAND TAMPER MINIMUM COVER = 5'-0".

SAND BORROW SPEC. COMPACTED IN 6" MAXIMUM LIFTS

MAXIMUM LIFTS USING A 75 LB. VIBRATORY

PLATE COMPACTOR, 4 PASSES MINIMUM

TYPICAL WATER SERVICE

PA VED

(NOT TO SCALE)

\UNPA VED |

WIDTH = D + 2'-0"

OR 3'-0" MIN.

WATER TRENCH

(NOT TO SCALE)

4" LOAM & SEED-

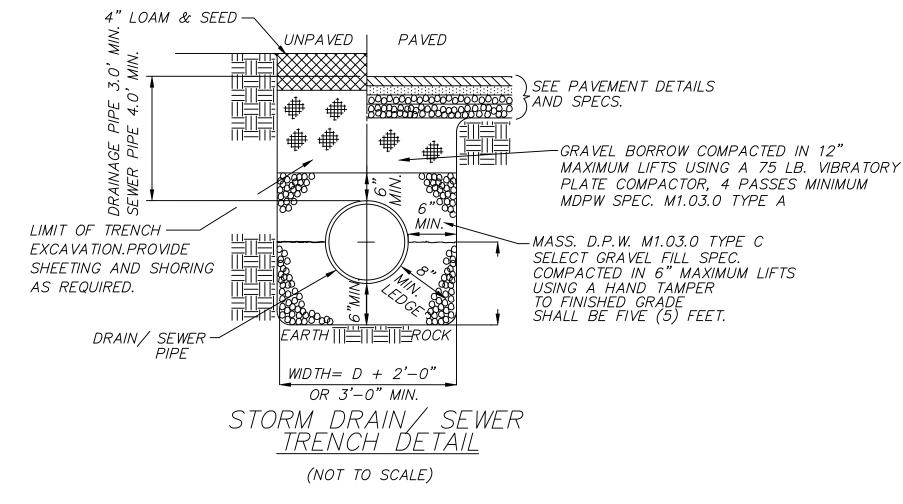
LIMIT OF TRENCH-

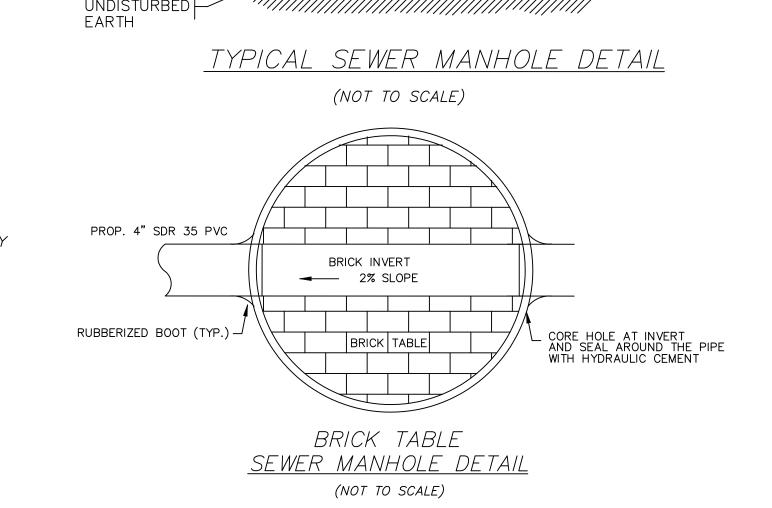
SHEETING AND

EXCA VA TION.PROVIDE

SHORING AS REQUIRED.

WATER PIPE-





1/2" PER FT.

] SLOPE (TYP.)

FOR REGISTRY OF DEEDS USE ONLY I DECLARE, TO THE BEST OF MY PROFESSIONAL KNOWLEDGE, INFORMATION, AND BELIEF, THAT THIS PLAN WAS PREPARED IN ACCORDANCE WITH THE RULES AND REGULATIONS OF THE REGISTERS OF DEEDS. JOHN D. SULLIVAN III, PE DATE READING COMMUNITY PLANNING & DEVELOPMENT COMMISSION

APPROVED ______, 20 ___

WOOD STAKES 7.7' O.C. AMOCO, 1380 SILT STOP (OR EQUAL), 12" DIAMETER 3.5' WIDE MULCH SOXX **⊸**FLOW 6"X 6" TRENCH WITH BACKFILL IN PLACE CROSS SECTION

> EROSION CONTROL BARRIER (NOT TO SCALE)



SEWER MANHOLE FRAME AND COVER SHALL BE TOWN OF

5 1/4"

READING STANDARD

MANHOLE SECTIONS SHALL

CONFORM TO ASTM SPEC C478

CONFORM TO ASTM A185 SPEC.

4000 PSI MINIMUM CONCRETE

LEVEL, STABLE AND

MDPW SPEC M1.03.0

COMPACTED GRAVEL BASE

COMPRESSIVE STRENGTH

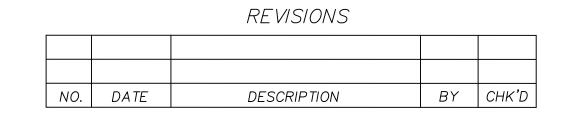
STEEL REINFORCEMENT SHALL

2-3 in. coarse Aggregate Geotextile fabric to stabilize foundation (especially important where wetness is anticipated)

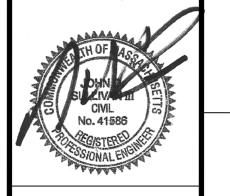
> TEMPORARY GRAVEL CONSTRUCTION <u>ENTRANCE/EXIT_PAD</u>

(NOT TO SCALE)

CONSTRUCT "TEMPORARY CONSTRUCTION ENTRANCE" AS SHOWN ON DETAIL PLAN PRIOR TO THE BEGINNING OF ANY CONSTRUCTION ACTIVITIES. ALL CONSTRUCTION VEHICLES SHALL EXIT THE SITE OVER THIS "TEMPORARY CONSTRUCTION ENTRANCE". THE CONTRACTOR SHALL USE THIS AREA TO REMOVE SOIL FROM THE TIRES OF CONSTRUCTION VEHICLES. "TEMPORARY CONSTRUCTION ENTRANCE" TO CONSIST OF SIX TO TWELVE INCHES OF TWO TO THREE INCH STONE.



DEFINITIVE SUBDIVISION PLAN "HAROLD AVENUE EXTENSION"



ADJUST RIM TO MATCH ROADWAY GRADE

MDPW SPEC M4.05.2 (RED BRICK)

CEMENT CONCRETE

MDPW SPEC M4.05.2

_ OUTLET INVERT ELEVATION

_ RIM ELEVATION

AND CROSS SLOPE WITH TWO (2) COURSES

(MINIMUM 2 COURSES, MAXIMUM 5 COURSES)

THE OUTLET INVERT SHALL BE AT

LEAST 2" BELOW THE INLET INVERT

OF RADIALLY PLACED RED BRICK AND PORTLAND CEMENT CONCRETE

THE CROWNS OF THE INLET PIPE AND OUTLET PIPE

DROP BETWEEN INLET AND OUTLET INVERTS REQUIRES

| TABLE AND INVERT SHALL BE FORMED OF RED SEWER

MDPW SPEC M4.02.00 et seq. (CÈMENT CONCRETE)

WITH CAST-IN FLEXIBLE SLEEVES (RUBBERIZED BOOTS

| PIPE TO MANHOLE CONNECTIONS SHALL BE MADE

BRICK AND 4000 PSI TYPE II PORTLAND CEMENT CONCRETE

(RED BRICK)

SHALL MATCH UNLESS THE REQUIRED 2" MINIMUM

THAT THE OUTLET CROWN BE INSTALLED LOWER

I JOINTS SHALL BE SEALED WITH BYTYL RUBBER

OR NEOPRENE RINGS AND PORTLAND TYPE II

SITE DEVELOPMENT PLAN LOCATED IN READING, MASSACHUSETTS (MIDDLESEX COUNTY)

> PREPARED FOR ZERO HAROLD AVENUE, LLC

SCALE: N.T.S. DATE: NOV. 4, 2023

<u>PREPARED BY</u>

SULLIVAN ENGINEERING GROUP, LLC P.O BOX 2004 WOBURN, MA 01888 (781) 854-8644

SHEET 5 OF 5

